



PCT

特許協力条約に基づいて公開された国際出願

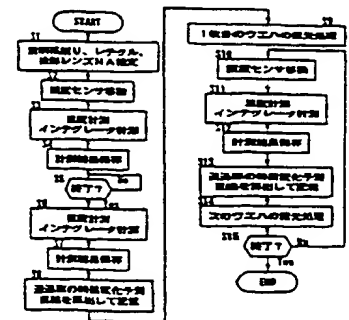
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(54)Title: PROJECTION ALIGNER, PROJECTION EXPOSURE METHOD, OPTICAL CLEANING METHOD AND METHOD OF FABRICATING SEMICONDUCTOR DEVICE

(54)発明の名称 投影露光装置、投影露光方法、光洗浄方法および半導体デバイスの製造方法

57) Abstract

A photosensitive wafer is exposed to light of a target illuminance regardless of the variation of time-varying transmittance of an optical system as follows. 20,000 pulses are idly shot before starting exposure of a first wafer (25). At the time of the first and 20,000th pulse laser oscillations, the transmittances of the optical system are calculated at the two moments by acquiring the output signals from an integrator sensor (10) and an illuminance sensor (28), and then a predictive line of time-varying transmittance is calculated from the two transmittances. When the exposure is started, the transmittance of the optical system is calculated at the elapsed time of exposure from the predictive line of time-varying transmittance, and the intensity of exposing light is controlled. The illuminance on the wafer can be compensated for depending on the actual variation of the transmittance. The accumulated quantity of exposing light incident to the wafer (25) is regulated to ensure a target exposure dose of the wafer (25) regardless of the variation in the transmittance of an illumination optical system or a projection optical system during exposure.



- 21 ... From illumination system transmittance, position, and size of photomask lens
- 22 ... from illumination system
- 23 ... Position illumination and integrated
- 24 ... from transmittance
- 25 ... end ?
- 26 ... measure illumination and integrated
- 27 ... from transmittance
- 28 ... Calculate and store predictive line of time-varying transmittance
- 29 ... expose first wafer
- 30 ... from illumination system
- 31 ... measure illumination and integrated
- 32 ... from transmittance
- 33 ... Calculate and store predictive line of time-varying transmittance
- 34 ... expose second wafer
- 35 ... end ?

## INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP98/03319

A. CLASSIFICATION OF SUBJECT MATTER  
Int.Cl<sup>6</sup> H01L21/027, G03F7/20

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
Int.Cl<sup>6</sup> H01L21/027, G03F7/20

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched  
Jitsuyo Shinan Koho 1972-1998  
Kokai Jitsuyo Shinan Koho 1972-1998

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	JP, 9-63948, A (Canon Inc.), 7 March, 1997 (07. 03. 97), Page 1 & KR, 97012982, A	44, 45, 50
A	JP, 6-204113, A (Canon Inc.), 22 July, 1994 (22. 07. 94), Page 1 (Family: none)	44, 45, 50
A	JP, 6-77107, A (Yamagata Nippon Denki K.K.), 18 March, 1994 (18. 03. 94), Page 1 (Family: none)	44, 45, 50

☐ Further documents are listed in the continuation of Box C.

☐ See patent family annex.

\* Special categories of cited documents:

"A" document defining the general state of the art which is not considered to be of particular relevance  
"E" earlier document but published on or after the international filing date  
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)  
"O" document referring to an oral disclosure, use, exhibition or other means  
"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention  
"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone  
"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art  
"&" document member of the same patent family

Date of the actual completion of the international search  
20 October, 1998 (20. 10. 98)

Date of mailing of the international search report  
27 October, 1998 (27. 10. 98)

Name and mailing address of the ISA/  
Japanese Patent Office

Authorized officer

Facsimile No.

Telephone No.

PCT

国際予備審査報告

(法第12条、法施行規則第56条)

[PCT36条及びPCT規則70]

PCT International Preliminary  
Examination Report

出願人又は代理人 の書類記号      FP98107PCT	今後の手続きについては、国際予備審査報告の送付通知（様式PCT/ IPEA/416）を参照すること。	
国際出願番号 PCT/J P 9 8 / 0 3 3 1 9	国際出願日 (日.月.年)      24.07.98	優先日 (日.月.年)      25.07.97
国際特許分類 (IPC) Int. Cl <sup>8</sup> H01L21/027      G03F7/20		
出願人 (氏名又は名称) 株式会社ニコン		

1. 国際予備審査機関が作成したこの国際予備審査報告を法施行規則第57条 (PCT36条) の規定に従い送付する。
2. この国際予備審査報告は、この表紙を含めて全部で 3 ページからなる。
- ☐ この国際予備審査報告には、附属書類、つまり補正されて、この報告の基礎とされた及び/又はこの国際予備審査機関に対してした訂正を含む明細書、請求の範囲及び/又は図面も添付されている。  
(PCT規則70.16及びPCT実施細則第607号参照)  
この附属書類は、全部で                      ページである。

3. この国際予備審査報告は、次の内容を含む。
- I ☒ 国際予備審査報告の基礎
- II ☐ 優先権
- III ☐ 新規性、進歩性又は産業上の利用可能性についての国際予備審査報告の不作成
- IV ☐ 発明の単一性の欠如
- V ☒ PCT35条(2)に規定する新規性、進歩性又は産業上の利用可能性についての見解、それを裏付けるための文献及び説明
- VI ☐ ある種の引用文献
- VII ☐ 国際出願の不備
- VIII ☐ 国際出願に対する意見

国際予備審査の請求書を受理した日 19.02.99	国際予備審査報告を作成した日 08.10.99	
名称及びあて先 日本国特許庁 (IPEA/J P) 郵便番号100-8915 東京都千代田区霞が関三丁目4番3号	特許庁審査官 (権限のある職員)  岩本 勉	2M 9355  印
電話番号 03-3581-1101 内線 3274		

## I. 国際予備審査報告の基礎

1. この国際予備審査報告は下記の出願書類に基づいて作成された。(法第6条(PCT14条)の規定に基づく命令に  
 応答するために提出された差し替え用紙は、この報告書において「出願時」とし、本報告書には添付しない。  
 PCT規則70.16, 70.17)

☒ 出願時の国際出願書類

- ☐ 明細書 第 \_\_\_\_\_ ページ、 出願時に提出されたもの  
 明細書 第 \_\_\_\_\_ ページ、 国際予備審査の請求書と共に提出されたもの  
 明細書 第 \_\_\_\_\_ ページ、 \_\_\_\_\_ 付の書簡と共に提出されたもの
- ☐ 請求の範囲 第 \_\_\_\_\_ 項、 出願時に提出されたもの  
 請求の範囲 第 \_\_\_\_\_ 項、 PCT19条の規定に基づき補正されたもの  
 請求の範囲 第 \_\_\_\_\_ 項、 国際予備審査の請求書と共に提出されたもの  
 請求の範囲 第 \_\_\_\_\_ 項、 \_\_\_\_\_ 付の書簡と共に提出されたもの
- ☐ 図面 第 \_\_\_\_\_ ページ/図、 出願時に提出されたもの  
 図面 第 \_\_\_\_\_ ページ/図、 国際予備審査の請求書と共に提出されたもの  
 図面 第 \_\_\_\_\_ ページ/図、 \_\_\_\_\_ 付の書簡と共に提出されたもの
- ☐ 明細書の配列表の部分 第 \_\_\_\_\_ ページ、 出願時に提出されたもの  
 明細書の配列表の部分 第 \_\_\_\_\_ ページ、 国際予備審査の請求書と共に提出されたもの  
 明細書の配列表の部分 第 \_\_\_\_\_ ページ、 \_\_\_\_\_ 付の書簡と共に提出されたもの

2. 上記の出願書類の言語は、下記に示す場合を除くほか、この国際出願の言語である。

上記の書類は、下記の言語である \_\_\_\_\_ 語である。

- ☐ 国際調査のために提出されたPCT規則23.1(b)にいう翻訳文の言語  
☐ PCT規則48.3(b)にいう国際公開の言語  
☐ 国際予備審査のために提出されたPCT規則55.2または55.3にいう翻訳文の言語

3. この国際出願は、ヌクレオチド又はアミノ酸配列を含んでおり、次の配列表に基づき国際予備審査報告を行った。

- ☐ この国際出願に含まれる書面による配列表  
☐ この国際出願と共に提出されたフレキシブルディスクによる配列表  
☐ 出願後に、この国際予備審査(または調査)機関に提出された書面による配列表  
☐ 出願後に、この国際予備審査(または調査)機関に提出されたフレキシブルディスクによる配列表  
☐ 出願後に提出した書面による配列表が出願時における国際出願の開示の範囲を超える事項を含まない旨の陳述書の提出があった  
☐ 書面による配列表に記載した配列とフレキシブルディスクによる配列表に記載した配列が同一である旨の陳述書の提出があった。

4. 補正により、下記の書類が削除された。

- ☐ 明細書 第 \_\_\_\_\_ ページ  
☐ 請求の範囲 第 \_\_\_\_\_ 項  
☐ 図面 図面の第 \_\_\_\_\_ ページ/図

5. ☐ この国際予備審査報告は、補充欄に示したように、補正が出願時における開示の範囲を越えてされたものと認められるので、その補正がされなかったものとして作成した。(PCT規則70.2(c) この補正を含む差し替え用紙は上記1.における判断の際に考慮しなければならず、本報告に添付する。)



## V. 新規性、進歩性又は産業上の利用可能性についての法第12条(PCT35条(2))に定める見解、それを裏付ける文献及び説明

## 1. 見解

新規性(N)

請求の範囲 1-61

有

請求の範囲

無

進歩性(I S)

請求の範囲 1-61

有

請求の範囲

無

産業上の利用可能性(I A)

請求の範囲 1-61

有

請求の範囲

無

## 2. 文献及び説明(PCT規則70.7)

## ・請求の範囲1-61

投影露光において、露光光と同じ波長に対する投影光学系の透過率を複数の異なる時点で測定し、測定された複数の透過率に基づいて投影光学系の透過率の時間変化特性を予測し、予測結果に基づいて投影露光を行うことは、国際調査報告で引用したいずれの文献にも記載されておらず、当業者にとって自明な事項でもない。

## SPECIFICATION

PROJECTION EXPOSURE APPARATUS, PROJECTION EXPOSURE METHOD,  
OPTICAL CLEANING METHOD AND METHOD OF FABRICATING  
SEMICONDUCTOR DEVICE

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This application is a continuation application of PCT  
Application No. PCT/JP98/03319 filed July 24, 1998.

The disclosures of the following priority  
10 applications are herein incorporated by reference:

Japanese Patent Application No. 9-199710

Japanese Patent Application No. 9-337104

Japanese Patent Application No. 10-67021

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## TECHNICAL FIELD

The present invention relates to a projection  
exposure apparatus employed to expose a pattern of an  
original such as a mask or a reticule (hereafter referred  
to as a mask) onto a photosensitive substrate such as a  
20 wafer during a photolithography process implemented during  
the fabrication of a semiconductor device such as an LSI,  
an image-capturing element such as a CCD, a liquid crystal  
display element, or a semiconductor device such as a thin  
film magnetic head, a projection exposure method utilizing  
25 this exposure apparatus, an optical cleaning method

employed to clean the optical systems in the projection exposure apparatus and a method of fabricating a semiconductor device.

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## BACKGROUND ART

Keeping pace with the increasingly higher integration achieved for semiconductor devices, significant progress has been made in the area of projection exposure apparatuses employed during the photolithography process that is crucial in fabrication of semiconductor devices. The resolving power achieved by a projection optical system mounted at a projection exposure apparatus is expressed through the relational expression  $R = k \times \lambda / NA$ , known widely as Rayleigh's formula. In this relational expression, R represents the resolving power of the projection optical system,  $\lambda$  represents the wavelength of the exposing light, NA represents the numerical aperture at the projection optical system and k represents a constant which is determined by process-related factors as well as the resolving power of the resist.

The resolving power required of the projection optical system to support higher integration in the semiconductor device may be achieved by reducing the wavelength of the light from the exposing light source or by increasing the numerical aperture at the projection

optical system as the relational expression above indicates. Thus, continuous efforts to achieve a higher NA value have been made. In recent years, exposure apparatuses that use a krypton fluoride excimer laser (KrF excimer laser) having an output wavelength of 248nm as an exposing light source with the numerical aperture at 0.6 or higher achieved at the projection optical system have been put into practical use to enable exposure of extremely fine patterns of down to  $0.25\mu\text{m}$ .

An argon fluoride excimer laser (ArF excimer laser) having an output wavelength of 193nm has been attracting much attention recently as a light source to replace the krypton fluoride excimer laser. Since it is expected that by realizing an exposure apparatus using this argon fluoride excimer laser as the exposing light source, ultra-fine processing down to  $0.18\mu\text{m} \sim 0.13\mu\text{m}$  will be possible, concentrated efforts are being made in research and development.

Since there are at present only two materials, i.e., synthetic silica glass and calcium fluoride (fluorite), that may be used to constitute the lenses while achieving a satisfactory transmittance in the wavelength range of the output wavelength (193nm) of the argon fluoride excimer laser, tireless efforts are being made to develop an optical material achieving sufficient transmittance and

sufficient internal consistency to be used in this type of exposure apparatus. Currently, synthetic silica glass achieves an internal transmittance of 0.995/cm or higher, and calcium fluoride has reached a point at which the level of internal absorption can be disregarded.

The choice of material to constitute the anti-reflection film that is coated on the surface of the optical material, too, is extremely limited compared to the range of materials from which selection can be made to constitute an anti-reflection film used in the output wavelength range (248nm) of the krypton fluoride excimer laser, and this also greatly restricts the degree of freedom afforded in design. However, thanks to the intense efforts made in development this problem, too, is being overcome. At present, the levels of losses at the individual lens surfaces (e.g., losses through the absorption of light by the coating, scattering of light, reflection at the interface of the coating and the optical material and reflection at the coating surface) have been lowered to 0.005 or less (light loss of 0.5% or less).

#### DISCLOSURE OF INVENTION

In wavelength ranges shorter than the wavelength of KrF excimer laser light, moisture and organic substances may adhere to the surfaces of the optical elements

constituting the optical systems (illumination optical system, projection optical system) in the projection exposure apparatus, resulting in a reduction in transmittance of the optical systems. This problem is attributable to gas trapped within the space enclosed by a plurality of optical elements or moisture and organic substances generated from the inner walls of the lens barrel or the like supporting the optical systems becoming adhered to the surfaces of the optical systems.

FIG. 17 illustrates time-varying transmittance characteristics in an optical system. The figure presents the optical system transmittance, which represents the ratio of the illuminance of the exposing light between the laser light source and the mask and the illuminance of the exposing light on the wafer measured over specific intervals while irradiating pulse laser light continuously from the laser light source during the laser irradiation and is calculated for each measuring time point. The figure also presents a similar optical system transmittance during a time period in which the laser is stopped that is obtained by irradiating laser over appropriate time intervals and calculated at each laser irradiation. As FIG. 17 illustrates, after the start of laser light irradiation, the transmittance gradually increases and when a specific length of time has elapsed,

a near-saturated state is achieved. This phenomenon of the optical system transmittance gradually recovering is due to moisture and organic substances adhering to the optical system surface being removed from the optical system surfaces by the laser irradiation. For this reason, it is conceivable to start an exposure operation after a near-saturated state of transmittance is achieved by irradiating exposing laser light over a specific period of time prior to the start of the exposure. However, this would cause a reduction in throughput. In addition, oscillation of the laser over a long period of time prior to the exposure would lead to poor durability of the laser light source and it is, therefore, not desirable. Furthermore, it is difficult to continuously irradiate exposing laser light at all times, including during replacement of the wafer or the mask.

A first object of the present invention is to provide a projection exposure method and a projection exposure apparatus that make it possible to sustain the illuminance of the exposing light on a photosensitive substrate at a target value at all times regardless of time-varying transmittance of the optical system.

A second object of the present invention is to provide a projection exposure method and a projection exposure apparatus that controls the accumulated light

quantity (exposure dose) of the exposing light on a photosensitive substrate at a correct value that corresponds to the sensitivity of the photosensitive substrate even when the transmittances at the illumination optical system and the projection optical system change.

A third object of the present invention is to provide an optical cleaning method for cleaning the optical systems by predicting time-varying transmittance at the illumination optical system and the projection optical system.

A fourth object of the present invention is to provide a method of fabricating a semiconductor device that achieves an improvement in the yield by exposing a circuit pattern or the like on a semiconductor substrate by predicting time-varying transmittance at the illumination optical system and the projection optical system.

A fifth object of the present invention is to provide a projection exposure method and a projection exposure apparatus that makes it possible to achieve a correct exposure dose at a photosensitive substrate in correspondence to changes in the transmittance occurring at the illumination optical system and the projection optical system even when conditions under which the photosensitive substrate is exposed, conditions under



which the mask is illuminated and the like are changed.

A sixth object of the present invention is to provide a projection exposure method and a projection exposure apparatus that prevent any fluctuation in the exposure  
5 dose occurring on a photosensitive substrate due to changes in the transmittance occurring at the illumination optical system and the projection optical system even when a change occurs in at least one of the following; the intensity distribution of the exposing light on the pupil  
10 surface of the projection optical system, i.e., the intensity distribution of a secondary light source within the illumination optical system (namely, the shape and size), the pattern on the mask to be transferred onto the photosensitive substrate and the numerical aperture at the  
15 projection optical system.

The present invention is applied in a projection exposure apparatus having an optical system that projects an image of a pattern illuminated by exposing light emitted by an exposing light source onto a photosensitive  
20 substrate with time-varying transmittance of the exposing light at the optical system and a projection exposure method employed in combination with the projection exposure apparatus. The objects described above are achieved by measuring the transmittance of the optical  
25 system with regard to light having a wavelength

substantially equal to the wavelength of the exposing light at a plurality of time points, predicting of time-varying transmittance characteristics of the optical system based upon the plurality of transmittances thus  
5 measured and projecting the pattern onto the photosensitive substrate based upon the results of the prediction.

It is desirable to measure the transmittance using exposing light emitted from the exposing light source.  
10 The plurality of time points at which the transmittance is measured may be a time point before the pattern is projected onto the photosensitive substrate, i.e., a time point before the light having the wavelength which is substantially the same as that of the exposing light is  
15 irradiated on the optical system and a time point after the light having the wavelength which is substantially the same as that of the exposing light is irradiated on the optical system over a specific length of time.  
Alternatively, the plurality of time points at which the  
20 transmittance is measured may constitute a time point before the image of the pattern illuminated by the exposing light is projected onto the photosensitive substrate and a time point after the image of the pattern illuminated by the exposing light is projected onto the  
25 photosensitive substrate.

The plurality of time points at which the measurement is performed may constitute, for instance, a time point before the image of the pattern illuminated by the exposing light is projected onto a single photosensitive substrate and a time point after the image of the pattern illuminated by the exposing light is projected onto the single photosensitive substrate. Alternatively, the plurality of time points for performing the measurement may constitute a time point before the image of a pattern illuminated by the exposing light is projected onto a specific area on a photosensitive substrate and a time point after the image of the pattern illuminated by the exposing light is projected onto the specific area. In this case, the plurality of time points may be time points before and after exposure processing performed on the exposure area of a single chip or time points before and after exposure processing performed on an exposure area corresponding to one shot.

If the optical system includes an illumination optical system that illuminates a pattern with exposing light and a projection optical system that projects the image of a pattern illuminated by the illumination optical system onto a photosensitive substrate, it is desirable to predict time-varying transmittance only at the optical system at which the transmittance fluctuates.

According to the present invention, the intensity of the exposing light irradiated onto the photosensitive substrate can be adjusted based upon predicted time-varying transmittance characteristics. Alternatively, the accumulated light quantity of the exposing light irradiated onto the photosensitive substrate can be controlled at a correct value that corresponds to the sensitivity of the photosensitive substrate based upon calculated time-varying transmittance characteristics.

10 In the method for controlling the accumulated light quantity in which the photosensitive substrate is made to move relative to the exposing light from the mask to pass through the projection optical system in synchronization with the movement of the mask relative to the exposing light during the process of emitting a pulse beam of exposure light from an exposing light source and projecting a pattern formed on the mask onto the photosensitive substrate, the accumulated light quantity of the exposing light can be controlled at a correct value corresponding to the sensitivity of the photosensitive substrate by adjusting at least one of the intensity of the exposing light entering the photosensitive substrate, the width of the exposing light on the photosensitive substrate relative to the traveling direction in which the photosensitive substrate moves, the traveling speed of the

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photosensitive substrate moving relative to the traveling direction and the oscillation frequency of the exposing light source, based upon the time-varying transmittance characteristics.

5        In addition, the present invention is adopted in a method of fabricating a semiconductor device by using a projection exposure apparatus having an optical system that projects the image of a pattern illuminated by exposing light emitted from an exposing light source onto  
10   a photosensitive substrate with the time-varying transmittance of the exposing light at the optical system. The objects described above are achieved by measuring the transmittance of light having a wavelength that is substantially equal to the wavelength of the exposing  
15   light at the optical system at a plurality of time points, predicting of time-varying transmittance characteristics at the optical system based upon a plurality of measured transmittances and projecting the image of the pattern onto the photosensitive substrate based upon the results  
20   of the prediction.

      Furthermore, the present invention is adopted in an optical cleaning method implemented to clean an optical system that projects the image of a pattern illuminated by exposing light from an exposing light source onto a  
25   photosensitive substrate provided in a projection exposure

apparatus with the transmittance of the exposing light at the optical system changing over time. The objects described earlier are achieved by measuring the transmittance of light having a wavelength substantially equal to the wavelength of the exposing light at the optical system at a plurality of time points and optically cleaning the optical system while predicting the time-varying transmittance characteristics at the optical system based upon a plurality of measured transmittances.

10       The projection exposure apparatus according to the present invention may comprise a mask illuminance detector that detects an illuminance of an exposing light irradiated on a mask from an exposing light source, a substrate illuminance detector that detects the illuminance of the exposing light on a photosensitive substrate, a means for prediction that predicts time-varying transmittance characteristics of the exposing light at the projection optical system by calculating the ratio of the illuminance of the exposing light irradiated on the mask detected by the mask illuminance detector and the illuminance of the exposing light irradiated on the substrate detected by the substrate illuminance detector a plurality of times and a control device that adjusts the accumulated light quantity of the exposing light entering the photosensitive substrate based upon the predicted

time-varying characteristics and the ratio of the two illuminances.

If the exposing light source is constituted of a pulsed light source, the control device may adjust at least, either the intensity of pulsed exposing light irradiated onto the photosensitive substrate or the number of pulses to ensure that the accumulated light quantity of the exposing light irradiated onto the photosensitive substrate achieves a correct value that corresponds to the type of the photosensitive substrate based upon the predicted time-varying characteristics and the ratio of the two illuminances.

The projection exposure method according to the present invention comprises a step in which time-varying transmittance characteristics of the exposing light at, at least, either an illumination optical system or a projection optical system are predicted by calculating the ratio of the illuminance of the exposing light emitted by an exposing light source and the illuminance of the exposing light on a photosensitive substrate a plurality of times and a step in which, at least, either the intensity of the pulsed exposing light entering the photosensitive substrate or the number of pulses is adjusted based upon the ratio of the illuminance of the exposing light emitted by the exposing light source and

the illuminance of the exposing light on the photosensitive substrate and the predicted time-varying transmittance characteristics.

The present invention is adopted in an exposure method implemented in a projection exposure apparatus having an illumination optical system that illuminates a mask on which a specific pattern is formed with exposing light emitted by an exposing light source and a projection optical system that projects the image of the pattern on the mask illuminated by the illumination optical system onto a photosensitive substrate, with the transmittance of the exposing light at, at least, either the illumination optical system or the projection optical system changing over time. The objects described earlier are achieved by adjusting the intensity of the exposing light irradiated onto the photosensitive substrate based upon the ratio of the illuminance of the exposing light emitted by the exposing light source and the illuminance of the exposing light on the photosensitive substrate and the time-varying characteristics of the exposing light transmittance at, at least, either the illumination optical system or the projection optical system. Or, if the exposing light source is constituted of a pulsed light source, the objects described earlier are achieved by adjusting at least, either the intensity of the exposing light entering



the photosensitive substrate or the number of pulses.

In a projection exposure apparatus in which the exposing light transmittance changes over time at its projection optical system alone among the illumination optical system and the projection optical system, the objects described above can be achieved by adjusting the accumulated light quantity of the exposing light entering the photosensitive substrate based upon the ratio of the illuminance of the exposing light emitted from the exposing light source and the illuminance of the exposing light on the photosensitive substrate and also based upon the time-varying characteristics of the exposing light transmittance at the projection optical system.

If the exposing light transmittance at the illumination optical system, too, changes over time, the objects described earlier can be achieved by adjusting the intensity of the exposing light emitted from the exposing light source based upon the time-varying characteristics of the exposing light transmittance in the entire optical system comprising the illumination optical system and the projection optical system and the ratio of the illuminances noted-above.

If the exposing light is a pulse beam, the accumulated light quantity of the exposing light can be controlled at a correct value that corresponds to the

sensitivity of the photosensitive substrate by adjusting, at least, either the intensity of the exposing light entering the photosensitive substrate or the number of pulse beams of the exposing light irradiated on a given spot on the photosensitive substrate.

The exposure method described above may be adopted on an exposure apparatus that transfers a pattern onto a photosensitive substrate by causing the substrate to travel relative to the exposing light from the mask passing through the projection optical system in synchronization with the movement of the mask relative to the exposing light. In such a scan-type exposure apparatus, the exposing light may be a pulse beam. When the exposing light is a pulse beam, the accumulated light quantity of the exposing light is controlled at a correct value that corresponds to the sensitivity of the photosensitive substrate by adjusting at least one of: the intensity of the exposing light entering the photosensitive substrate, the width of the exposing light on the photosensitive substrate relative to the traveling direction in which the photosensitive substrate moves, the traveling speed at which the photosensitive substrate moves in the traveling direction and the oscillation frequency of the exposing light source.

The present invention is adopted in a projection

exposure apparatus having an illumination optical system that illuminates a mask at which a specific pattern is formed with exposing light emitted by an exposing light source and a projection optical system that projects the image of the pattern at the mask illuminated by the illumination optical system onto a photosensitive substrate with the exposure light transmittance at the projection optical system changing over time. The objects described earlier are achieved by providing a mask illuminance detector that detects the illuminance of the exposing light irradiated on the mask from the exposing light source, a substrate illuminance detector that detects the illuminance of the exposing light on the photosensitive substrate, a storage device that stores in memory time-varying characteristics of the exposing light transmittance at the projection optical system and a control device that adjusts the accumulated intensity of the exposing light entering the photosensitive substrate based upon the ratio of the illuminance of the exposing light irradiated on the mask detected by the mask illuminance detector and the illuminance of the exposing light irradiated onto the photosensitive substrate detected by the substrate illuminance detector and the time-varying characteristics stored in the storage device. In addition, the control device may adjust at least,

either the intensity or the number of the exposing light irradiated onto the photosensitive substrate to ensure that the accumulated light quantity of the exposing light irradiated onto the photosensitive substrate achieves a correct value that corresponds to the photosensitive substrate.

If the exposing light transmittance at the illumination optical system also changes over time in this projection exposure apparatus, it is desirable to store in memory the time-varying characteristics of the exposing light transmittance in the entire optical system comprising the illumination optical system and the projection system in the storage device. The storage device is capable of storing a plurality of sets of time-varying transmittance characteristics of the exposing light in correspondence to various exposure conditions. If a given set of exposure conditions does not match the exposure conditions stored in memory in the storage device, the transmittance is calculated through an interpolation operation performed on the time-varying characteristics stored in memory. The exposure conditions in this context refer to the illumination conditions of the illumination optical system (e.g., the diameter of the variable aperture stop at the illumination system, a modified illumination or a normal illumination etc.), the type of

the mask and the numerical aperture at the projection optical system.

It is to be noted that if the exposing light is continuous light, either the intensity of the exposing light on the photosensitive substrate or the length of the irradiation period may be adjusted, or both may be adjusted. If the exposing light is pulsed light, either the pulse intensity of the exposing light on the photosensitive substrate or the number of pulses may be adjusted, or both may be adjusted. When exposure is achieved by scanning exposing light onto an exposure area on the photosensitive substrate that corresponds to the pattern area of the mask, at least one of: the intensity of the exposing light, the width of the exposing light along the scanning direction, the scanning speed of the substrate along the scanning direction and the oscillation frequency of the light source may be adjusted.

As explained above, according to the present invention, exposure performed on a photosensitive substrate is controlled based upon predicted time-varying transmittance characteristics of the exposing light calculated for, or based upon time-varying transmittance characteristics of the exposing light corresponding to various exposure conditions that are stored in advance. Thus, even when the transmittance at the illumination

optical system or the projection optical system fluctuates during an exposure operation or while the apparatus is in a stopped state, the photosensitive substrate can be exposed correctly. For instance, the illuminance on the photosensitive substrate can be controlled at a correct value, or the accumulated light quantity (exposure dose) of the exposing light on the photosensitive substrate can be controlled at a correct value that corresponds to the sensitivity of the photosensitive substrate at all times.

10 In addition, according to the present invention, even when conditions under which the photosensitive substrate is exposed, conditions under which the mask is illuminated and the like are changed, or even when, at least one of: the intensity distribution of the exposing light on the pupil surface at the projection optical system, i.e., the intensity distribution of a secondary light source within the illumination optical system (the shape and size), the pattern on the mask to be transferred on the photosensitive substrate and the numerical aperture at the projection optical system, is changed, fluctuations in the exposure dose on the photosensitive substrate due to changes occurring in the transmittances at the illumination optical system and the projection optical system can be prevented from occurring by calculating the predicted time-varying transmittance characteristics that

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20

25

correspond to the specific changes or by storing in memory in advance time-varying transmittance characteristics that correspond the specific changes.

Furthermore, the predicted time-varying transmittance characteristics may be calculated by irradiating light having a wavelength substantially equal to the wavelength of the exposing light prior to the actual exposure operation so that the predicted time-varying transmittance characteristics can be calculated concurrently during optical cleaning performed prior to the exposure processing to prevent any reduction in throughput.

Moreover, according to the present invention, in which a semiconductor device is fabricated by calculating predicted time-varying transmittance characteristics and controlling the exposure operation based upon the predicted characteristics, an improvement is achieved in the production yield of semiconductor devices.

#### BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 illustrates a schematic structure of the projection exposure apparatus according to the present invention;

FIG. 2 illustrates the variable aperture stops formed at the turret plate shown in FIG. 1;

FIG. 3 illustrates the variable aperture stops in the

illumination optical system formed at the pupil position of the projection optical system within the projection exposure apparatus illustrated in FIG. 1;

FIG. 4 presents a graph illustrating the relationship  
5 between the length of the exposure period and the transmittance;

FIG. 5 is a flowchart of the procedure through which a pattern is exposed on a wafer by calculating the predictive line of time-varying transmittance;

10 FIG. 6 is a block diagram of the feedback system employed to control the exposing light on the wafer at a target illuminance value;

FIG. 7 presents a graph illustrating the relationship between the length of exposure period and the  
15 transmittance;

FIG. 8 is a flowchart of another example of the procedure through which a pattern is exposed on a wafer by calculating the predictive line of time-varying transmittance;

20 FIG. 9 is a flowchart of yet another example of the procedure through which a pattern is exposed on a wafer by calculating the predictive line of time-varying transmittance;

FIG. 10 is a flowchart of yet another example of the  
25 procedure through which a pattern is exposed on a wafer by



calculating the predictive line of time-varying transmittance;

FIG. 11 is a plan view of a reticule provided with a pericle in which a transparent area for measurement is  
5 formed;

FIG. 12 is an explanatory view illustrating time-varying transmittance characteristics that vary in correspondence to the type of reticule;

FIG. 13 is an explanatory view illustrating time-  
10 varying transmittance characteristics in correspondence to the size of the variable aperture stop;

FIG. 14 is a flowchart of the procedure implemented to store in advance the time-varying transmittance characteristics in correspondence to exposure conditions;

15 FIG. 15 is an explanatory view illustrating the transmittance measured after an exposure operation which has been interrupted due to wafer replacement is resumed;

FIG. 16 is an explanatory view illustrating the transmittance measured after an exposure operation which  
20 has been interrupted due to reticule replacement is resumed; and

FIG. 17 is an explanatory view illustrating the transmittance that fluctuates in correspondence to varying lengths of the exposure period.

## BEST MODE FOR CARRING OUT THE INVENTION

(First embodiment in which exposure processing is performed by predicting time-varying transmittance characteristics)

5       The following is an explanation of the first embodiment of the present invention given in reference to the drawings. FIG. 1 illustrates a schematic structure of the projection exposure apparatus according to the present invention. As shown in FIG. 1, laser light constituted of almost parallel light flux is emitted by an ArF excimer  
10       laser light source 1 that oscillates a pulsed light having an output wavelength of, for instance, 193nm, and the laser light is guided to a light transmitting window 3 at a main unit of the projection exposure apparatus via a  
15       shutter 2. The shutter 2 closes the illumination light path during a replacement of the wafer or the reticule, for instance, thereby causing self-oscillation at the light source 1 to stabilize (adjust) beam characteristics that include at least one of: the central wavelength, the  
20       wavelength width and the intensity of the pulsed light.

      The main unit of the projection exposure apparatus is housed inside a chamber 100 and is controlled to maintain a constant temperature. The laser light having passed through the light transmitting window 3 is shaped into  
25       laser light achieving a specific cross sectional outline

at a beam shaping optical system 4, passes through one of a plurality of ND filters (ND1 in FIG. 1) having different transmittances (extinction rates) from each other that are provided at a turret plate TP to be reflected by a  
5 reflecting mirror 5 and then is guided to a fly-eye lens 6 constituting an optical integrator. The fly-eye lens 6 is constituted by bundling together a number of lens elements, with numerous of light source images (secondary light sources) the number of which corresponds to the number of  
10 lens elements constituting the fly-eye lens 6 formed at the emission surfaces of the lens elements.

In this embodiment, the turret plate TP holds six ND filters ND1 ~ ND6 (only ND1 and ND2 shown in the figure), and by causing the turret plate TP to rotate with a motor  
15 MT1, the six ND filters may be positioned within an illumination optical system in an interchangeable manner. One of the six ND filters is selected depending upon the sensitivity of the resist on the wafer 25, the inconsistency in the oscillation intensity of the light  
20 source 1, the accuracy of control of the exposure dose implemented on the wafer 25 and the like. In addition, an appropriate ND filter is selected in correspondence to the number of pulse beams (the number of exposure pulses) to be irradiated on a given point on the wafer 25 during the  
25 process of scanning exposure. The number of exposure

pulses in this context refers to the number of pulse beams that are irradiated at a given point on the wafer 25 while the point crosses an area that is conjugate with an illumination area on a reticule 16 defined by a variable-  
5 field stop 12 relative to a projection optical system 23 (i.e., an area on which an image of a portion of the pattern at the reticule 16 present inside the illumination area is projected) along its scanning direction.

Instead of the turret plate TP in FIG. 1, two plates  
10 each having a plurality of slits may be provided facing opposite each other to adjust the intensity of the pulsed light by moving the two plates relative to each other along the direction in which the slits are formed.

The light source 1 oscillates pulsed light in  
15 response to a trigger pulse transmitted by a light source control circuit 45 (see FIG. 6), and the light source control circuit 45 adjusts the voltage applied to the light source 1 (charging voltage) to adjust the intensity of the pulsed light emitted from the light source 1. It  
20 is to be noted that the light source control circuit 45 controls the light source 1 in response to commands from a main controller (control circuit) 40 that implements overall control of the entire projection exposure apparatus.

25 In the embodiment, the intensity of the pulsed light

on the reticule 16, i.e., on the wafer 25, can be adjusted through, at least, either through adjustment of the oscillation intensity at the light source 1 implemented by the light source control circuit 45 or through adjustment of the transmittance (extinction rate) of the pulsed light implemented at the turret plate TP.

In the embodiment, the mirror 5 is caused to rotate (oscillate) by a motor MT2 while the wafer 5 is being exposed using the image of the pattern at the reticule 16 by causing the reticule 16 and the wafer 25 to move in synchronization with each other, as disclosed in Japanese Laid-Open Patent Publication No. H7-142354, for instance. Thus, interference fringes such as speckles move within the illumination area on the reticule 16 defined by the variable-field stop 12 during scanning exposure, to achieve near consistency in the distribution of the accumulated light quantity of the pulsed light on the wafer 25. At this time, the interference fringes are moved at least once while one point on the reticule 16 crosses the illumination area along the scanning direction. In addition, it is desirable to oscillate the reflecting mirror 5 so that the interference fringes move along the scanning direction and also relative to the direction perpendicular to the scanning direction of the reticule 16 within the illumination area. When moving the

interference fringes along the scanning direction within the illumination area, the angle over which the reflecting mirror 5 is swung between pulsed light emissions, i.e., the distance over which the interference fringes are moved, should be determined by taking into consideration the distance over which the reticule 16 moves between the pulsed light emissions so that the positional relationship between the one point on the reticule 16 and the interference fringes changes while the one point crosses the illumination area.

While one fly-eye lens 6 is provided in this embodiment, a fly-eye lens constituting a second optical integrator may be provided between the reflecting mirror 5 and the turret plate TP as disclosed in, for instance, Japanese Laid-Open Patent Publication No. H1-259533. Alternatively, a rod-shaped optical member that achieves internal reflection may be employed as an optical integrator in place of the fly-eye lens.

As detailed later, at the positions at which the numerous secondary light sources are formed by the fly-eye lens 6, a turret plate 7 having a plurality of aperture stops 7a ~ 7h with, at least, either different shapes or different sizes from one another is provided. The turret plate 7, which is driven by a motor 8 to rotate, is inserted inside the optical path of the illumination

optical system with one aperture stop selected in  
correspondence to the pattern at the reticule 16 to be  
transferred onto the wafer 25. The turret plate 7 and the  
motor 8 constitute an illumination system variable  
5 aperture stop device .

The light beams from the numerous secondary light  
sources formed by the fly-eye lens 6 are then branched  
into two optical paths by a beam splitter 9 after they  
pass through the variable aperture stop at the turret  
10 plate 7, and the reflected light is guided to an  
integrator sensor (photoelectric detector) 10 where the  
illuminance of the illumination light is detected. A  
signal that corresponds to the detected illuminance is  
input to the control circuit 40. The transmitted light,  
15 on the other hand, travels through a relay lens 11, the  
variable field stop 12 that defines a rectangular opening  
and a relay lens 13 to be reflected at a reflecting mirror  
14 and then is condensed at a condenser optical system 15  
constituted of a refractive optical element such as a  
20 plurality of lenses. Thus, almost consistent illumination  
of the illumination area on the reticule 16 defined by the  
opening at the variable field stop 12 is achieved in a  
superimposed manner. Then the image of the circuit  
pattern on the reticule 16 is formed on the wafer 25 by  
25 the projection optical system 23, and the resist applied

onto the wafer 25 is exposed, thereby transferring the circuit pattern image onto the wafer 25.

The illumination area on the reticule 16 defined by the variable field stop 12 is set to have a width along the direction in which the reticule 16 is scanned that is smaller than the width of the pattern area and a width along the direction perpendicular to the scanning direction that is larger than the width of the pattern area. In addition, the illumination area extends inside the circular image field at the projection optical system 23 along its diameter around an optical axis AX of the projection optical system 23.

By moving at least one of the blades constituting the variable field aperture 12 with the motor MT3, the shape and size of the rectangular opening at the variable field stop 12 can be varied. In particular by changing the width of the rectangular opening in the direction of the short side, the width of the illumination area along the scanning direction on the reticule 16 is changed, which makes it possible to adjust the accumulated light quantity (exposure dose) of a plurality of pulse beams irradiated on one point on the wafer through scanning exposure, since the number of pulse beams irradiated on the point while it crosses the rectangular area which is conjugate with the illumination area on the reticule 16 relative to the



projection optical system 23 along the scanning direction is changed.

As explained above, in the embodiment, the oscillation frequency at the light source 1 can be changed  
5 by a trigger pulse transmitted from the light source control circuit 45, and thus, the accumulated light quantity of a plurality of pulse beams irradiated on one point on the wafer 25 during scanning exposure can be adjusted. In addition, by changing the scanning speed at  
10 which the wafer 25 (and the reticule 16) is scanned, too, the accumulated light quantity of the plurality of pulse beams irradiated on one point on the wafer 25 during scanning exposure can be adjusted, since the number of pulse beams irradiated on the spot while it crosses the  
15 projection area which is conjugate with the illumination area on the reticule 16 along the scanning direction is changed in correspondence to changes in the oscillation frequency or the scanning speed, as explained above.

In a scanning-type projection exposure apparatus, at  
20 least, either the intensity of the pulsed light on the wafer 25 or the number of pulse beams irradiated on the individual points on the wafer 25 during scanning exposure is adjusted to control the accumulated light quantity (exposure dose) of the plurality of pulse beams irradiated  
25 on each point within an area of the wafer 25 that is

exposed by the image of the pattern at the reticule 16 at a correct value that corresponds to the sensitivity of the photoresist on the wafer 25.

As explained above, the oscillation intensity at the light source 1 and the transmittance (extinction rate) of the pulsed light can be changed independently of each other in the embodiment, and by changing at least, either the oscillation intensity or the transmittance, the intensity of the pulsed light on the wafer 25 can be adjusted to achieve optimization of the exposure dose. According to the present invention, optimization of the exposure dose may be achieved by adjusting the number of pulse beams irradiated on each point on the wafer 25 instead of achieving exposure dose optimization through the adjustment of the pulsed light intensity as described above. In other words, in the embodiment, the width of the opening at the variable field stop 12, i.e., the width of the pulsed light on the wafer 45 (corresponds to the projection area explained earlier) along the scanning direction, the oscillation frequency at the light source 1 and the scanning speed at which the wafer 25 is scanned can be changed independently, and by changing at least one of: the pulsed light width, the oscillation frequency and the scanning speed, the number of pulse beams irradiated onto each point on the wafer 25 can be adjusted. It is

obvious that optimization of the exposure dose can be achieved by adjusting both the intensity of the pulsed light on the wafer 25 and the number of pulse beams irradiated on each point on the wafer 25.

5       Namely, in the embodiment, by adjusting at least one of the oscillation intensity at the light source, the transmittance of the pulsed light (extinction rate), the pulsed light width on the wafer 25, the oscillation frequency at the light source 1 and the scanning speed at  
10       which the wafer 25 is scanned, the exposure dose at each point on the wafer 25 can be set at a correct value or the accuracy of control of the exposure dose can be set within a required accuracy range (e.g.,  $\pm 1 \sim 2\%$ ).

      The entire projection optical system 23 in the  
15       embodiment is constituted of optical elements such as refracting lenses, and an aperture stop  $E_p$  is provided at a position at which the pupil (entrance pupil) of the projection optical system 23 is located. This aperture stop  $E_p$  may be constituted of a mechanism that is capable  
20       of changing its size so that the numerical aperture at the projection optical system can be varied, and in such a case, the aperture stop  $E_p$  in the projection optical system and the variable aperture stops 7a - 7h in the illumination optical system are provided at positions that  
25       are optically conjugate with each other.

The reticule 16 is securely held at a reticule stage 18 by a reticule holder 17. The reticule stage 18 is provided on a base 22 to make linear movement along a plane perpendicular to the sheet upon which FIG. 1 is presented. A mirror 21 is provided at the reticule holder 17, and laser light from a laser interferometer 20 is reflected by the mirror 21 to enter the laser interferometer 20, which then measures the position of the reticule stage 18. This positional information is input to the control circuit 40 and, based upon the positional information, the control circuit 40 drives a reticule stage drive motor 19 to control the position of the reticule 16 and the speed of the reticule 16 during a scanning exposure operation.

The wafer 25 is securely held at a wafer stage 27 by a wafer holder 26. The wafer stage 27 makes a linear movement along a plane perpendicular to the sheet upon which FIG. 1 is presented. A mirror 31 is provided at the wafer stage 27, and laser light from a laser interferometer 30 is reflected by the mirror 31 to enter the laser interferometer 30, which then measures the position of the wafer stage 27. This positional information is input to the control circuit 40 and, based upon the positional information, the control circuit 40 drives a wafer stage drive motor 29 to control the

position of the wafer 25 and the speed of the wafer 25 during a scanning operation. An illuminance sensor (photoelectric detector) 28 is provided on the wafer stage 27 to detect the illuminance of the exposing light irradiated on the wafer 25. The detection signal from the illuminance sensor 28 is input to the control circuit 40.

In the projection exposure apparatus in the embodiment, the illumination optical system is placed in an inert gas atmosphere such as nitrogen gas. For this reason, an inert gas supply device that supplies inert gas to the casing (not shown) of the illumination optical system and an inert gas discharge device that discharges contaminated inert gas from the casing are provided, as disclosed in, for instance, Japanese Laid-Open Patent Publication No. H6-260385. In addition, inert gas such as nitrogen gas is supplied to a plurality of spaces formed between the plurality of optical members constituting the projection optical system 23, and contaminated inert gas is discharged from the plurality of spaces. To achieve this, an inert gas supply device 41 and an inert gas discharge device 42 are provided, with the gas supply device 41 supplying inert gas such as dry nitrogen into the projection optical system 23 via a pipe 43 and the discharge device 42 discharging the gas inside the projection optical system 23 via a pipe 44. It is to be

noted that the inert gas use in the projection exposure apparatus does not need to be nitrogen, and selection may be made from gases including helium and argon.

Next, the variable aperture stop device that changes the numerical aperture at the illumination optical system (i.e., the shape and the size of the secondary light source) in the projection exposure apparatus is explained. As illustrated in FIG. 1, when the numerical aperture at the illumination optical system, which is determined by a principal light beam  $R_i$  parallel to the optical axis  $AX$  from the outermost edge (outermost diameter) of the aperture stop inserted in the optical path of the illumination optical system at the turret plate 7 is represented by  $NA_i (= \sin \theta_i)$  and the numerical aperture at the projection optical system 23 toward the illumination optical system determined by a principal light beam  $R_o$  parallel to the optical axis  $AX$  from the outermost edge (outermost diameter) of the aperture stop  $Ep$  of the projection optical system 23 is represented by  $NA_o (= \sin \theta_o)$ , the value of  $\sigma$  as a coherence factor is defined as follows.

$$\sigma = NA_i / NA_o \quad (1)$$

Since the aperture stop  $Ep$  provided at the position at which the pupil (entrance pupil) of the projection optical system 23 is located and the variable aperture

stops at the turret plate 7 of the illumination optical system are optically conjugate and the image of the variable aperture stop (image of the secondary light source) is formed at the pupil of the projection optical system 23, the value of  $\sigma$  as the maximum coherence factor can be defined as follows, with D7 representing the diameter of the image of the variable aperture stop and D23 representing the diameter of the aperture stop Ep at the projection optical system 23.

10 
$$\sigma = D7 / D23 \quad (2)$$

Normally, the value  $\sigma$  at the projection exposure apparatus is set within a range of 0.3~0.8 during the photolithography process. In the embodiment, the turret plate 7 shown in FIG. 1 is provided with a plurality of aperture stops 7a~7h illustrated in FIG. 2, and one of the aperture stops is selected to suit a specific purpose of use as detailed later.

As illustrated in FIG. 2, eight aperture stops 7a~7h are formed at the turret plate 7, constituted of a transparent substrate such as quartz. The 5 aperture stops 7a and 7e~7h have round openings and are used to forcibly change the value  $\sigma$  with the three aperture stops 7e, 7f and 7g employed during an actual exposure operation and the remaining two aperture stops 7a and 7h employed during an optical cleaning operation. Optical cleaning is

a process in which contaminants such as moisture and organic substances adhering to the lens surfaces are removed from the lens surfaces by irradiating laser to improve the transmittance.

5       The three aperture stops 7b-7d with modified openings are provided to be used during an exposure operation to improve the resolving power (focal depth) of the projection optical system 23. The aperture stops 7c and 7d each has a ring band opening, and the ring band ratio  
10 (the ratio of the internal diameter and the external diameter of the ring band opening) of one is different from the ring band ratio of the other. The remaining aperture stop 7b has four decentered openings provided to form four decentered secondary light sources.

15       The turret plate 7 having the 8 aperture stops 7a ~ 7h is rotated by the motor 8 shown in FIG. 1, so that one aperture stop among the 8 aperture stops, i.e., the stop having the desired aperture opening shape is positioned adjacent to the exit surface of the fly-eye lens 6. In  
20 other words, it is set at the focal plane on the exit side where secondary light sources are formed by the fly-eye lens 6. The drive of the motor 8 is controlled by the control circuit 40.

FIG. 3 illustrates the images of the aperture stops  
25 7a and 7e-7h having round openings of different sizes



formed on the aperture stop Ep within the projection optical system 23. Each aperture stop is now explained in detail in (1)~(5) below.

(1) When the aperture stop 7e having the smallest round opening is set on the illumination light path, the numerical aperture  $NA_i$  at the illumination optical system is at the smallest, and at this time, the image of the aperture stop 7e having an opening diameter  $D_{7e}$  is formed inside the aperture stop Ep having an opening diameter  $D_{23a}$  with the value  $\sigma$  set to 0.4. In other words, a relationship whereby  $\sigma = D_{7e} / D_{23a} = NA_i / NA_o = 0.4$  is achieved. Consequently, when the aperture stop 7e is set on the illumination light path, the pattern at the reticule 16 can be transferred onto the wafer 25 with the value  $\sigma$  set to 0.4.

(2) When the aperture stop 7f having a round opening larger than that of the aperture stop 7e is set on the illumination light path, the numerical aperture  $NA_i$  at the illumination optical system becomes larger than that when the aperture stop 7e is set on the illumination light path. At this time, the image of the aperture stop 7f having the opening diameter  $D_{7f}$  is formed inside the aperture stop Ep having an opening diameter  $D_{23a}$  with the value  $\sigma$  set to 0.6. In other words, a relationship whereby  $\sigma = D_{7f} / D_{23a} = NA_i / NA_o = 0.6$  is achieved. Consequently, when the

aperture stop 7f is set on the illumination light path, the pattern at the reticule 16 can be transferred onto the wafer 25 with the value  $\sigma$  set to 0.6.

(3) When the aperture stop 7g having a round opening  
5 larger than that of the aperture stop 7f is set on the illumination light path, the numerical aperture  $NA_i$  at the illumination optical system becomes larger than that when the aperture stop 7f is set on the illumination light path. At this time, the image of the aperture stop 7g having the  
10 opening diameter  $D_{7g}$  is formed inside the aperture stop  $Ep$  having an opening diameter  $D_{23a}$  with the value  $\sigma$  set to 0.8. In other words, a relationship whereby  $\sigma = D_{7g} / D_{23a} = NA_i / NA_o = 0.8$  is achieved. Consequently, when the aperture stop 7g is set on the illumination light path,  
15 the pattern at the reticule 16 can be transferred onto the wafer 25 with the value  $\sigma$  set to 0.8.

(4) When the aperture stop 7h having a round opening larger than that of aperture stop 7g is set on the illumination light path, the numerical aperture  $NA_i$  at the  
20 illumination optical system becomes larger than that when the aperture stop 7g is set on the illumination light path. At this time, the image of the aperture stop 7h having the opening diameter  $D_{7h}$  that is equal to the opening diameter  $D_{23a}$  of the aperture stop  $Ep$  is formed with the value  $\sigma$   
25 set to 1.0. In other words, a relationship whereby  $\sigma =$

$D7h/D23a = NA_i / NA_o = 1.0$  is achieved. Consequently, when the aperture stop 7h is set on the illumination light path, the illumination light flux can be guided over the effective diameters of the optical elements constituting the condenser optical system 15 in the illumination optical system, over the effective diameters of the optical elements such as lenses constituting the projection optical system 23 and even over areas well beyond the effective diameters of these optical elements. Thus, moisture, organic substances and the like adhering to the surfaces of these optical elements can be eliminated through the optical cleaning effect achieved by the exposure illumination light flux.

(5) When the aperture stop 7a having a round opening larger than that of the aperture stop 7h is set on the illumination light path, the numerical aperture  $NA_i$  at the illumination optical system becomes larger than that when the aperture stop 7h is set on the illumination light path. At this time, the image of the aperture stop 7a having the opening diameter  $D7a$  is formed to contain the aperture stop  $Ep$  having the opening diameter  $D23a$  with the value  $\sigma$  set to 1.2. In other words, a relationship whereby  $\sigma = D7a/D23a = NA_i / NA_o = 1.2$  is achieved. Consequently, when the aperture stop 7a is set on the illumination light path, the illumination light flux can be guided over to the lens

peripheries well beyond the effective diameters of the optical elements as well as over the effective diameters of the optical elements constituting the condenser optical system 15 in the illumination optical system and over the effective diameters of the optical elements such as lenses constituting the projection optical system 23. Thus, the advantage of optically cleaning moisture, organic substances and the like adhering to the surfaces of these optical elements can be fully realized.

10       The operation achieved in the embodiment is explained. First, as illustrated in FIG. 1, inert gas such as dry nitrogen is supplied from the gas supply device 41 into the projection optical system 23 via the pipe 43, and when the optical projection system is fully charged with inert gas, the gas in the projection optical system 23 is discharged to the outside via the pipe 44 by the discharge device 42. The entire optical path through which the exposing light travels in the illumination optical system, too, is designed to be a sealed structure as in the projection optical system 23, and likewise, inert gas such as dry nitrogen is supplied and charged into the illumination optical system in a similar manner and the gas inside the illumination optical system is discharged by a discharge device.

25       It is desirable to keep the atmosphere among optical

such as lens chambers elements in a dry, cleaned state at all times by operating the gas supply device 41 and the discharge device 42 during exposure. However, the supply device 41 and the discharge device 42 may be stopped after  
5 replacing the gas in the spaces formed between the optical elements such as lens chambers prior to the exposure operation. The same principle applies with respect to the illumination optical system.

Next, employing a reticule loading mechanism (not  
10 shown), the reticule 16 on which a pattern to be transferred is drawn is delivered and placed onto the reticule stage 18. At this time, the position of the reticule 16 is measured with a reticule alignment system (not shown) and the reticule 16 is set at a specific  
15 position with a reticule position control circuit (not shown) based upon the results of the measurement.

Before starting the exposure operation, a predictive line of time-varying transmittance at the projection optical system 23 (time-varying transmittance  
20 characteristics) as indicated by C1 in FIG. 4 is calculated. FIG. 4 is a graph with the horizontal axis representing the exposure time and the vertical axis representing the transmittance. The transmittance in FIG. 4 is the transmittance at the optical system extending  
25 from a half mirror 9 that branches the exposing light into

an integrator sensor 10 to the wafer surface (hereafter, this optical system is referred to as the transmittance measurement optical system).

First, by driving the laser light source 1 after the  
5 illuminance sensor 28 is positioned on the optical axis of the projection optical system 23, an idle emission of 20,000 pulses, for instance, is performed. The illuminance of the exposing light may be measured at the integrator sensor 10 and the illuminance sensor 28 in  
10 synchronization with, for instance, the first pulse. Then the ratio  $LW/LI$  of the output  $LI$  from the integrator sensor 10 and the output  $LW$  from the illuminance sensor 28 is calculated. This ratio represents the transmittance  $P0$  at the exposure start in FIG. 4. Next, the illuminance of  
15 the exposing light may be measured at the integrator sensor 10 and the illuminance sensor 28 in synchronization with, for instance, the 20,001st pulse. Then the ratio  $LW/LI$  of the output  $LI$  from the integrator sensor 10 and the output  $LW$  from the illuminance sensor 28 is calculated.  
20 The ratio represents the transmittance  $P1$  at the exposure time point  $t1$  in FIG. 4.

Through the self-cleaning effect achieved through the idle emission of laser pulses, moisture and organic substances adhered on the surfaces of the transmittance  
25 measurement optical system that includes the projection

optical system 23 are removed from the lens surfaces and, as a result, the transmittance of the transmittance measurement optical system improves to achieve  $P1 > P0$ .

By connecting these two transmittances  $P0$  and  $P1$  with a  
5 line, the predictive line  $C1$  of time-varying transmittance is obtained.

FIG. 5 is a flowchart of the procedure through which exposure is performed while calculating a predictive line of time-varying transmittance characteristics. In step  $S1$ ,  
10 the variable aperture stop at the illumination optical system, the reticule type and the numerical aperture  $NA$  at the projection optical system are determined and input. Based upon the input data, the turret plate 7 is driven by the motor 8 to rotate, the aperture stop that forms a  
15 secondary light source having a corresponding shape and size is inserted in the illumination light path, and the numerical aperture  $NA$  at the projection optical system 23 is adjusted through the aperture stop  $Ep$ . In addition, the reticule 16 that has been selected is delivered from  
20 the reticule library and is set on the reticule stage 18.

In step  $S2$ , the wafer stage 27 is moved to position the illuminance sensor 28 on the optical axis of the projection optical system 23. In step  $S3$ , the laser light source 1 is driven to emit laser light (idle emission),  
25 the illuminance  $LI$  of the exposing light reflected by the

mirror 9 is detected by the integrator sensor 10 and the illuminance LW of the exposing light on the wafer stage 27 is detected by the illuminance sensor 28. In step S4, the results of these detections are stored in memory as first  
5 detected illuminances. When it is decided in step S5 that the idle emission of 20,000 pulses has been completed, the operation proceeds to step S6. In step S6, the 20,001st pulse of the pulse laser is emitted, the illuminance LI of the exposing light reflected by the mirror 9 is detected  
10 by the integrator sensor 10 and the illuminance LW of the exposing light at the wafer stage 27 is detected by the illuminance sensor 28. In step S7, the results of these detections are stored in memory as the last detected illuminances of the idle emission.

15 Then, in step S8, the predictive line of time-varying transmittance is calculated based upon the first detected illuminances and the last detected illuminances. This predictive line is achieved through approximation by calculating the transmittance P0 representing the ratio LW  
20 / LI of the first detected illuminances and the transmittance P1 representing the ratio LW / LI of the last detected illuminances and then connecting these points P0 and P1. This predictive line of time-varying transmittance may be stored as a linear function or may be  
25 stored in a storage device 57 which is to be detailed



later as a table of transmittances relative to exposure time.

When the predictive line of time-varying transmittance C1 is determined in this manner, a first wafer 25 is placed to face opposite the optical axis of the projection optical system 23 and exposure is started in step S9 in FIG. 5. A resist, which is a photosensitive material, is applied in advance on the surface of the wafer 25 onto which the pattern at the reticule 16 is to be transferred, and the wafer 25 is delivered in this state by the wafer loading mechanism (not shown) to be placed on the wafer stage 27. The wafer 25 is aligned on the wafer stage 27 and becomes securely held. No pattern is present on the wafer 25 placed on the wafer stage 27 at the time of the first pattern transfer, and it is set at a specific position on the wafer stage 27, e.g., a position determined in correspondence to the external diameter of the wafer 25. Then, the pattern is transferred onto the wafer 25. This transfer is a scanning type transfer (step-and-scan method) in which a portion of the pattern of the reticule 16 is selectively illuminated by the variable field stop (reticule blind) 12, the reticule 16 is moved by the reticule stage 18 relative to the illumination area defined by the variable field stop 12 and the wafer 25 is moved by the wafer stage 27 relative

to the projection area which is conjugate with the illumination area relative to the projection optical system 23 in synchronization with the relative movement of the reticule 16. Alternatively, the transfer may be  
5 achieved through a step-and-repeat method in which the entire pattern area on the reticule 16 to be transferred is illuminated and transferred at once.

FIG. 6 is a block diagram of feedback control implemented to control the intensity of the laser light at  
10 a target illuminance on the wafer according to the present invention, which may be realized within the control circuit 40 in the form of software or hardware. The target illuminance at the wafer which is determined in correspondence to the sensitivity characteristics of the  
15 resist and the like is set at a target value setting circuit 51. As explained earlier, the integrator sensor 10 outputs the detection signal LI which corresponds to the illuminance of the exposing light made consistent by the fly-eye lens 6, and the illuminance sensor 28 outputs  
20 the detection signal LW that corresponds to the illuminance of the exposing light on the wafer stage 27. Prior to the start of an exposure operation, the illuminance sensor 28 is moved onto the optical axis AX of the projection optical system 23, and the measured value  
25 LI at the integrator sensor 10 and the measured value LW

at the illuminance sensor 28 are held at a sample hold circuit 52. The ratio of the detection signal LI from the integrator sensor 10 and the detection signal LW from the illuminance sensor 28 (output LW from sensor 28/ output LI from sensor 10) is calculated at a divider 53, and a gain  $\alpha$  calculating unit 54 calculates the gain by multiplying LW / LI by a specific coefficient K1. Then, during the exposure operation, a multiplier 55 multiplies the output signal from the integrator sensor 10 by the gain and outputs an estimated actual illuminance LPR. In other words, when the measured value at the integrator sensor 10 is 100 and the illuminance on the wafer 25 is 50 at the start of exposure, for instance, the estimated actual illuminance LPR represents an estimated value of the illuminance at the wafer achieved by multiplying the gain, which has been calculated by multiplying the ratio 50/100 by the specific coefficient K1, by the output signal from the integrator 10, output during the exposure. Hence, the gain  $\alpha$  is set as an optimal value for a situation in which there is no fluctuation in the transmittance.

The estimated actual illuminance LPR calculated by multiplying the detection signal from the integrator sensor 10 by the gain  $\alpha$  at the multiplier 55 is further multiplied by a gain  $\beta$  at a multiplier 56, to calculate a

corrected estimated actual illuminance LPRC on the wafer.  
The gain  $\beta$  is calculated as described below.

As explained earlier, the predictive line of time-varying transmittance that is determined in advance is  
5 stored in the storage device 57. A timer 58 measures the  
length of time elapsed after the start of exposure, and  
the storage device 57 is accessed depending upon the  
length of the measured time to read out the transmittance.  
The results of the readout are input to a gain  $\beta$   
10 calculating unit 59, which multiplies the transmittance  
read out by a specific coefficient K2 to calculate the  
gain  $\beta$ . For instance, when the transmittance is 80%, the  
gain  $\beta$  is set at  $0.8 \times K2$ .

The signal LPRC achieved by multiplying the detection  
15 signal from the integrator sensor 10 by the gains  $\alpha$  and  $\beta$   
indicates an estimated value of the actual illuminance at  
the wafer stage 27, and is input to a deviation calculator  
60. The deviation calculator 60 calculates the deviation  
between the target illuminance at the wafer output by the  
20 target value setting circuit 51 and the corrected  
estimated actual illuminance, inputs the deviation thus  
calculated to a PID arithmetic circuit 61 to perform a PID  
arithmetic operation and sends the results of the PID  
operation to the light source control circuit 45 to  
25 control the light source 1 or adjust its oscillation

intensity.

Assuming that the pattern image is currently projected on the wafer between the time points  $t_1$  and  $t_2$  in FIG. 4, the transmittance used during the exposure operation performed between the time points  $t_1$  and  $t_2$  is calculated by using the predictive line C1 based upon the length of time elapsed during this period (exposure time).

When the exposure of the first wafer 25 is completed in step S9 (at the time point  $t_2$  in FIG. 4) in FIG. 5, a transmittance P2 is calculated from the ratio  $LW / LI$  of the illuminances detected by the integrator sensor 10 and the illuminance sensor 28 at the time point  $t_2$  in steps S10 ~ S12, as in steps S2 ~ S4 explained earlier, and the transmittance P2 is stored in memory before the operation proceeds to step S13. In step S13, the transmittance P1 at the time point  $t_1$  and the transmittance P2 at the time point  $t_2$  is connected as in step S8, and predictive line C2 of time-varying transmittance is calculated as shown in FIG. 4.

Next, in step S14, exposure of the next (second) wafer 25 starts. During the exposure of the second wafer, too, the transmittance is calculated based upon the length of time elapsed between the time points  $t_2$  and  $t_3$  using the predictive line C2 in a manner similar to that in which the first wafer was exposed, and the exposure

regression line or a regression curve that is achieved by not directly connecting the calculated transmittances may be used. The approximation may be achieved through polynomial approximation, exponential approximation, 5 indicial approximation, modified indicial approximation or the like.

A method that may be adopted to calculate a predictive line of time-varying transmittance using transmittances corresponding to three or more points as 10 described above is now explained in detail in reference to FIG. 7. FIG. 7, which is similar to FIG. 4, presents a predictive line C11 of time-varying transmittance calculated by using transmittances at three time points prior to the exposure of the second wafer. An approximate 15 predictive line C11 is calculated through the method of least squares using the following formula (3), based upon three sets of data  $(t_0, P_0)$ ,  $(t_1, P_1)$  and  $(t_2, P_2)$  respectively indicating the transmittance  $P_0$  at the time point  $t_0$ , the transmittance  $P_1$  at the time point  $t_1$  and 20 the transmittance  $P_2$  at the time point  $t_2$  in FIG. 7.

$$P(t) = M \times t + I \dots (3)$$

where,

$$M = \frac{\sum_{j=0}^2 (t_j - \bar{t})(P_j - \bar{P})}{\sum_{j=0}^2 (t_j - \bar{t})^2}$$

$$I = \bar{P} - M \times \bar{t}$$

$$\bar{t} = \sum_{j=0}^2 t_j$$

$$\bar{P} = \sum_{j=0}^2 P_j$$

A transmittance P3 at a time point t3 at which the  
 5 exposure of the second wafer ends is calculated as  
 explained earlier, and before starting the exposure of a  
 third wafer, an approximate line C21 is calculated through  
 the method of least squares using the following formula  
 (4), based upon three sets of data (t1, P1), (t2, P2) and  
 10 (t3, P3) respectively indicating the transmittance P1 at  
 the time point t1, the transmittance P2 at the time point  
 t2 and the transmittance P3 at the time point t3 in FIG. 7.

$$P(t) = M \times t + I \dots (4)$$

where,

$$15 \quad M = \frac{\sum_{j=1}^3 (t_j - \bar{t})(P_j - \bar{P})}{\sum_{j=1}^3 (t_j - \bar{t})^2}$$

$$I = \bar{P} - M \times \bar{t}$$

$$\bar{t} = \sum_{j=1}^3 t_j$$

$$\bar{P} = \sum_{j=1}^3 P_j$$

Subsequently, predictive line of time-varying

transmittance is calculated using the most recent three sets of data as described above when exposing a fourth and subsequent wafers as well and the exposure control is implemented in conformance to the predictive line of time-varying transmittance.

In addition, while the predictive line of time-varying transmittance is calculated after the exposure of the first wafer ends by measuring the transmittance before the exposure of the next wafer starts, a predictive line may be calculated in units of two wafers, three wafers or the like if error can be tolerated. In other words, the exposure quantity control may be implemented by using a transmittance calculated in conformance to a common predictive line that pertains to a plurality of wafers.

FIG. 8 is a flowchart of an exposure procedure implemented in such a case.

FIG. 8 is a flowchart of an example of a procedure that may be implemented when exposure is performed by calculating a predictive line of time-varying transmittance every plurality of wafers instead of every wafer. By assigning the same reference numbers to steps identical to those in FIG. 5, the explanation will mainly focus on differences from the flowchart in FIG. 5. The predictive line of time-varying transmittance calculated in step S8 is commonly used until it is decided in step



S21 that exposure processing has been performed on m wafers. If it is decided in step S21 that the exposure processing on the m wafers has been completed, a decision is made in step S22 as to whether or not the entire exposure processing has been completed. If it is decided that the entire processing has been completed, all the processing in FIG. 8 ends. If a negative decision is made in step S22 and exposure processing is to be executed on a wafer continuously, a new predictive line of time-varying transmittance is calculated using the previous transmittance and the current transmittance in steps S10 ~ S13. Then, the operation proceeds to step S9, in which exposure processing is performed while implementing exposure quantity control using the new predictive line of time-varying transmittance.

Thus, since a predictive line of time-varying transmittance is calculated every plurality of wafers if fluctuations in the transmittance are not great in the procedure in FIG. 8, exposure can be performed at a correct exposure quantity with a high degree of accuracy without greatly reducing the throughput.

If the transmittance fluctuates to an unacceptable degree while exposing a single wafer, it is desirable to calculate a predictive line every chip or every two chips. FIG. 9 is a flowchart of an exposure procedure that may be

implemented in such a case.

FIG. 9 is a flowchart of an example of a procedure that may be implemented when exposure is performed by calculating a predictive line of time-varying transmittance every N chips on a given wafer instead of every wafer. By assigning the same reference numbers to steps identical to those in FIG. 5, the explanation will mainly focus on differences from the flowchart in FIG. 5. The predictive line of time-varying transmittance calculated in step S8 is commonly used until exposure processing on N chips is determined to be completed in step S31. A decision is made in step S32 as to whether or not the exposure processing on the given wafer has been completed. If a negative decision is made, a new predictive line of time-varying transmittance is calculated using the previous transmittance and the current transmittance in steps S10 - S13. Then the operation proceeds to step S31, in which exposure processing is performed on the next N chips while implementing exposure quantity control using the new predictive line of time-varying transmittance. If it is decided in step S32 that the exposure processing on the given wafer has been completed, a decision is made in step S33 as to whether or not the entire exposure processing has been completed. If it is decided that the entire

processing has been completed, all the processing in FIG. 9 ends. If a negative decision is made in step S33 and exposure processing is to be executed on a new wafer continuously, the operation proceeds to step S10 ~ S13 to  
5 calculate a new predictive line of time-varying transmittance and then the processing in step S31 and in subsequent steps is executed. Thus, since a predictive line of time-varying transmittance is calculated for every N chips that are being exposed on a single wafer when  
10 fluctuations in the transmittance are great, exposure can be performed at a correct exposure quantity with a high degree of accuracy. It is to be noted that the number of chips that use a common predictive line of time-varying transmittance should be set at value equal to 1 or greater  
15 as appropriate.

Furthermore, if fluctuations in the transmittance become small enough to be tolerated, the exposure quantity control using a predictive line of time-varying transmittance may be stopped. FIG. 10 is a flowchart of  
20 an exposure procedure that may be implemented in such a case. By assigning the same reference numbers to steps identical to those in FIG. 5, explanation will mainly focus on differences from FIG. 5.

In FIG. 10, unless it is decided in step S41 that the  
25 transmittance is equal to or greater than a preset

reference value, the operation proceeds to step S44, and by using the predictive line of time-varying transmittance which has been calculated immediately before, exposure processing on the next wafer is performed in step S14. If  
5 it is decided in step S41 that the transmittance is equal to or greater than the preset reference value, the operation proceeds to step S42 to set the flag, and then in step S43, the value of the gain  $\beta$  is determined by assuming that there will be no subsequent time-varying  
10 transmittance. For instance, as explained earlier in reference to FIG. 6, in case that the gain  $\beta$  is determined by multiplying the coefficient K2 by the transmittance, a specific transmittance determined in step S41 is used to determine the gain  $\beta$ . Then, exposure processing is  
15 performed on the next wafer in step S14 and if it is decided in step S15 that the entire exposure processing has not been completed as yet, a decision is made in step S45 with respect to the status of the flag. If the flag is set, the operation proceeds to step S14, whereas if it  
20 is not set, the operation proceeds to step S10.

Thus, by implementing the procedure in FIG. 10, which does not require calculation of a predictive line of time-varying transmittance when the transmittance is equal to or greater than a specific value, the length of processing  
25 time can be reduced to achieve an improvement in throughput.

It is necessary to bear in mind the following points when measuring the illuminance at the wafer 25 with the illuminance sensor 28. The transmittance at the reticule is affected by the pattern density at the reticule 16, and  
5 if the position of the reticule changes every time the illuminance sensor 28 measures the illuminance at the wafer 25, the transmittance cannot be measured accurately. Thus, it is necessary to set the reticule 16 at the same position on the reticule stage 18 when measuring the  
10 illuminance at the wafer 25 with the illuminance sensor 28.

In addition, the transmittance at a so-called white reticule having a low ratio of the pattern area (the area corresponding to the light blocking portion (chrome)) against the reticule surface area (the area corresponding  
15 to the rectangular portion where the pattern is formed) greatly differs from the transmittance at a so-called black reticule, having a high ratio of the pattern area against the reticule surface area. Since the transmittance of the exposing light being irradiated is  
20 small at a black reticule, the quantity of light entering the illuminance sensor 28 may be below the sensitivity threshold of the sensor 28. In this case, the illuminance on the wafer 25 effectively cannot be measured, and therefore, a predictive line of time-varying transmittance  
25 cannot be calculated.

As a solution, a reticule 16 having a transparent area for measurement RA formed outside the reticule pattern area RP, as illustrated in FIG. 11, may be used to measure the illuminance at the wafer stage by moving the illuminance sensor 28 to a position that is conjugate with the transparent area RA relative to the projection optical system 23 when measuring the illuminance at the wafer 25. PE indicates the position at which the pericle frame is located. The shape and the quantity of the transparent area are not limited to those in the example in FIG. 11. It is to be noted that the illuminance sensor 28 may be placed at a position that is conjugate with an area of the reticule 16 where the pattern density is low relative to the projection optical system 23 without using the transparent area RA. Alternatively, an opening through which the illumination light passes may be provided at the reticule stage itself. Or a measurement may be performed by the illuminance sensor 28 by causing the reticule stage 18 to completely move away from the illumination light path.

(Second embodiment in which exposure processing is performed based upon pre-stored time-varying transmittance characteristics)

While exposure processing is performed by predicting time-varying transmittance characteristics in the first

embodiment explained above, in the second embodiment, exposure processing is performed using time-varying transmittance characteristics that are stored in memory prior to exposure.

5        Since the entire structure of the exposure apparatus and the circuit that sets the exposing light at a target value are identical to those illustrated in FIG. 1 or FIG. 6, a detailed explanation thereof is omitted. It is to be noted that the method for setting time-varying  
10       transmittance characteristics to be stored in the storage device 57 in FIG. 6 in the second embodiment differs from the method employed in the first embodiment. Thus, the method for setting time-varying transmittance  
15       characteristics stored in the storage device 57 in FIG. 6 is first explained.

      The contents of memory in the storage device 57 are now explained. FIG. 12 illustrates time-varying transmittance characteristics at the projection optical system 23 in correspondence to different types of  
20       reticules, with the solid line RW representing the characteristics of a so-called white reticule having a low ratio of the pattern area (the area of the light blocking portion (chrome)) against the reticule surface area (the area of the rectangular portion where the pattern is  
25       formed) and the broken line RB representing the

characteristics of a so-called black reticule having a high ratio of pattern area against reticule surface area. Since the white reticule achieves a larger transmittance of the exposing light illuminating the reticule compared to the black reticule, it demonstrates excellent self-cleaning effect on the projection optical system 23, manifests a steeper rise of the transmittance compared to the black reticule and tends to have a higher transmittance saturation level.

Different tendencies manifest in the time-varying transmittance characteristics in correspondence to varying exposure conditions as well as in correspondence to different types of reticules in use. When the aperture stops 7e, 7f and 7g for regular illumination are used at the variable aperture stop device, tendencies represented by the solid line 7g, the one-point chain line 7f and the broken line 7e in FIG. 13 manifest. In the figure, the solid line T7e represents the characteristics achieved by using the aperture stop 7e, the one-point chain line T7f represents the characteristics achieved by using the aperture stop 7f and the broken line T7g represents the characteristics achieved by using the aperture stop 7g. It is to be noted that the size of  $\sigma$  corresponds to the size of the aperture stop as long as the numerical aperture NA at the projection optical system 23 is



constant, and the aperture stops 7g, 7f and 7e in FIG. 13 correspond to a large  $\sigma$ , a medium  $\sigma$  and a small  $\sigma$  respectively. While the time-varying characteristics manifest different tendencies in correspondence to the numerical apertures NA at the projection optical system 23 as well, a tendency whereby steeper rise characteristics and a higher transmittance saturation is observed when the numerical aperture NA is large, since the exposing light entering the optical system located toward the wafer relative to the aperture stop Ep in the projection optical system becomes greater.

Since the time-varying transmittance characteristics are different between the ring band openings 7c and 7d at the turret plate 7 for a modified illumination in correspondence to the internal diameters and the external diameters of the ring bands, these characteristics are measured and stored in advance.

The time-varying transmittance characteristics in FIGS. 12 and 13 that are obtained through advance measurement performed under various exposure conditions are stored together with sample time points in the storage device 57 in FIG. 6, and when a specific exposure conditions are determined, the table that corresponds to the exposure conditions is referenced to read out the transmittance in accordance with the length of time

elapsed after the start of the exposure operation.

The conditions under which the wafer 25 is to be exposed using the image of the pattern at the reticule 16 is constituted of a combination of the type of pattern, the intensity distribution of the secondary light sources constituted of a plurality of light source images (shape and size), which is the condition under which the reticule is illuminated that is determined in correspondence to the pattern type, and the numerical aperture at the projection optical system 23 determined in correspondence to the pattern type.

If the exposure conditions do not match any of the exposure conditions stored in advance at the storage device 57, the table of the closest exposure condition may be used to calculate the transmittance through an interpolation operation. For instance, if the ratio of pattern area against reticule surface area is halfway between the ratio achieved by a white pattern and that achieved by a black pattern, the transmittance can be determined by correcting the transmittance read from the time-varying transmittance characteristics of either the white pattern or the black pattern in correspondence to the rate of pattern area ratio.

The time-varying transmittance characteristics are explained above in reference a situation in which exposure

condition factors change within a single exposure condition. However, there are bound to be a numerous exposure conditions resulting from optimal combinations of a plurality of types of individual exposure conditions, including reticule type, the illumination method adopted at the illumination optical system, the numerical aperture at the projection optical system and the like. Thus, it is difficult to measure in advance time-varying characteristics in correspondence to all conceivable exposure conditions. As a result, in reality, time-varying characteristics are measured in correspondence to a plurality of typical exposure conditions, and if the actual exposure conditions do not fit any of the exposure conditions stored in the storage device 57, the gain  $\beta$  is calculated through an interpolation operation to predict the time-varying transmittance characteristics under the particular exposure conditions.

Time-varying transmittance characteristics are measured and stored in correspondence to a plurality of exposure conditions each constituted of a combination of factors, i.e., the reticule type, the shape and size of the secondary light sources (the illumination condition) and the numerical aperture at the projection optical system 23 in this example. However, the exposure conditions do not need to be constituted of a combination

of these three factors. Instead, at least two of these three factors, e.g., the reticule type and the illumination condition may be combined to constitute a single exposure condition and a plurality of such exposure  
5 conditions may be measured and stored.

Next, the operation achieved in the embodiment is explained. First, as illustrated in FIG. 1, inert gas such as dry nitrogen is supplied from the gas supply device 41 into the projection optical system 23 via the  
10 pipe 43. When the projection optical system is fully charged with inert gas, the gas in the projection optical system 23 is discharged to the outside via the pipe 44 by the discharge device 42. The entire optical path through which the exposing light travels in the illumination  
15 optical system, too, is designed to be a sealed structure as in the projection optical system 23, and likewise, inert gas such as dry nitrogen is supplied and charged into the illumination optical system in a similar manner and the gas inside the optical system is discharged by the  
20 discharge device.

It is desirable to hold the atmosphere among optical elements such as lens chambers in a dry, cleaned state at all times by operating the gas supply device 41 and the discharge device 42 during exposure. However, the supply  
25 device 41 and the discharge device 42 may be stopped after

replacing the gas in the spaces formed between the optical elements such as the lens chambers prior to the exposure operation. The same principle applies with respect to the illumination optical system.

5       Next, employing a reticule loading mechanism (not shown), the reticule 16 on which a pattern to be transferred is drawn is delivered and placed onto the reticule stage 18. At this time, the position of the reticule 16 is measured with a reticule alignment system  
10 (not shown) and the reticule 16 is set at a specific position with a reticule position control circuit (not shown) based upon the results of the measurement.

A resist, which is a photosensitive material, is applied in advance on the surface of the wafer 25 onto  
15 which the pattern at the reticule 16 is to be transferred, and the wafer 25 is delivered in this state by a wafer loading mechanism (not shown) to be placed on the wafer stage 27. The wafer 25 is aligned on the wafer stage 27 and becomes securely held. No pattern is present on the  
20 wafer 25 placed on the wafer stage 27 at the time of the first pattern transfer, and it is set at a specific position on the wafer stage 27, e.g., a position determined in correspondence to the external diameter of the wafer 25. Then, the pattern is transferred onto the  
25 wafer 25. This transfer is the so-called scanning type

transfer (step-and-scan method) in which a portion of the pattern of the reticule 16 is selectively eliminated by the variable field stop (reticule blind) 12, moving the reticule 16 with the reticule stage 18 relative to the illumination area defined by the variable field stop 12 and the wafer 25 is moved by the wafer stage 27 relative to the projection area which is conjugate with the illumination area relative to the projection optical system 23 in synchronization with the relative movement of the reticule 16. Alternatively, the transfer may be achieved through a step-and-repeat method in which the entire pattern area on the reticule 16 to be transferred is illuminated and transferred at once .

Since a pattern is present at least on the wafer 25 at the time of a second or subsequent pattern transfer onto the wafer 25, the position of the pattern that has already been transferred on the wafer 25 is measured by employing a wafer alignment system (not shown) to measure a mark added to the pattern and based upon the results of the measurement, the positions of the reticule stage 18 and the wafer stage 27 are controlled to achieve a specific positional relationship between the pattern that has already been transferred onto the wafer 25 and the pattern to be transferred.

To continue with the explanation given in reference

to FIG. 6, prior to the start of an exposure operation, the illuminance sensor 28 is moved onto the optical axis AX of the projection optical system 23, and the measured value LI at the integrator sensor 10 and the measured value LW at the illuminance sensor 28 are held at the sample hold circuit 52. The ratio of the detection signal LI from the integrator sensor 10 and the detection signal LW from the illuminance sensor 28 (output LW from sensor 28/ output LI from sensor 10) is calculated at the divider 53, and the gain  $\alpha$  calculating unit 54 calculates the gain  $\alpha$  by multiplying LW/LI by a specific coefficient K1. Then, during the exposure operation, the multiplier 55 multiplies the output signal from the integrator sensor 10 by the gain  $\alpha$  and outputs an estimated actual illuminance LPR. In other words, when the measured value at the integrator sensor 10 is 100 and the illuminance on the wafer 25 is 50 at the start of exposure, for instance, the estimated actual illuminance LPR represents an estimated value of the illuminance at the wafer achieved by multiplying the gain  $\alpha$ , which has been calculated by multiplying the ratio 50/100 by the specific coefficient K1, by the output signal from the integrator 10, output during the exposure.

The estimated actual illuminance LPR calculated by multiplying the detection signal from the integrator

sensor 10 by the gain  $\alpha$  at the multiplier 55 is further multiplied by a gain  $\beta$  at the multiplier 56, to calculate a corrected estimated actual illuminance LPRC on the wafer. The gain  $\beta$  is calculated as described below.

5       The storage device 57, having stored the time-varying transmittance characteristics at the illumination optical system and the projection optical system determined in advance, is accessed according to a specific length time elapsed after the start of exposure measured by the timer  
10   58 to read out the transmittance. The results of the readout are input to the gain  $\beta$  calculating unit 59, which multiplies the transmittance readout by a specific coefficient K2 to calculate the gain  $\beta$ . For instance, when the transmittance is 80%, the gain  $\beta$  is set at 0.8 X  
15   K2.

      The signal LPRC achieved by multiplying the detection signal from the integrator sensor 10 by the gains  $\alpha$  and  $\beta$  indicates an estimated value of the actual illuminance at the wafer stage 27, and is input to the deviation  
20   calculator 60. The deviation calculator 60 calculates the deviation between the target illuminance at the wafer output by the target value setting circuit 51 and the corrected estimated actual illuminance, inputs the deviation thus calculated to the PID arithmetic circuit 61  
25   to perform a PID arithmetic operation and sends the



results of the PID arithmetic operation to the light source control circuit 45 to control the light source 1 or adjust its oscillation intensity.

A procedure that may be implemented to store time-varying transmittance characteristics obtained through advance measurement in the storage device 57 is explained in reference to FIG. 14. In step S1, the variable aperture stop at the illumination optical system, the reticule type and the numerical aperture NA at the projection optical system are determined and input. Based upon the input data, the turret plate 7 is driven by the motor 8 to rotate, the aperture stop that forms secondary light sources having the shape and the size corresponding to its type is inserted in the illumination light path, and the numerical aperture NA at the projection optical system 23 is adjusted through the aperture stop Ep. In addition, the reticule 16 that has been selected is delivered from the reticule library and is set on the reticule stage 18.

In step S2, the wafer stage 27 is moved to position the illuminance sensor 28 on the optical axis of the projection optical system 23. In step S3, the laser light source 1 is driven to emit laser light, the illuminance of the exposing light at the illumination optical system is detected by the integrator sensor 10 and the illuminance

of the exposing light on the wafer stage 27 is detected by the illuminance sensor 28. In step S4, the results of these detections are stored in memory together with the measuring time point. Steps S3 and S4 are repeated until  
5 it is decided in step S5 that the measurement has been completed, and when it is decided in step S5 that the measurement has been completed, the program goes to step S6 in which the transmittances corresponding to the individual measuring time points are calculated and stored  
10 in memory based upon the detection results obtained at the integrator sensor 10 and the detection results obtained at the illuminance sensor 28 through the measurement. Thus, a table representing the time-varying characteristics as illustrated in FIG. 12 or FIG. 13 is stored in memory.

15 Next, an interruption in an exposure operation due to a wafer replacement or the like is explained in reference to FIG. 15. In FIG. 15, changes in the characteristics of transmittance occurring over time when a wafer delivery starts at a time point t1, a delivery of the next wafer  
20 ends and an exposure operation start at a time point t2 is indicated by the one-point chain line. As the laser light irradiation is interrupted at the time point t1, the self-cleaning of the projection optical system 23 and the illumination optical system is interrupted as well. As a  
25 result, suspended contaminants within the projection

optical system 23 and the illumination optical system become re-adhered to the surfaces of the optical elements in the optical systems or the transmittances (of the optical materials) of the optical elements themselves fluctuate to result in a reduction in the transmittances of the projection optical system 23 and the illumination optical system. When the laser light irradiation is resumed at the time point  $t_2$ , self-cleaning of the optical elements starts again to result in an increase in the transmittances.

Thus, at the time point  $t_2$  at which the laser light irradiation is resumed, the illuminance sensor 28 is moved onto the optical axis of the projection optical system 23 to measure the illuminance of the exposing light at the wafer stage 27 and, at the same time, the illuminance of the exposing light at the illumination optical system is detected by the integrator sensor 10. The transmittance at the time point  $t_2$  is calculated based upon the results of the measurement at the two sensors, and a time point  $t_0$  that corresponds to the transmittance is determined based upon the time-varying transmittance characteristics represented by the solid line. Then, when the exposure is resumed, the timer 58 that measures the length of exposure time elapsing after the exposure start is reset at the time point  $t_0$ . Consequently, when the exposure operation

starts, the storage device 57 references the table representing the time-varying transmittance characteristics in FIG. 15 to calculate the gain  $\beta$  by reading out the data corresponding to the length of time counted on the timer 58.

Next, an interruption in the exposure operation due to a reticule replacement is explained in reference to FIG. 16. FIG. 16 shows the characteristics diagram in FIG. 12 that illustrates the time-varying transmittance characteristics at a white reticule and at a black reticule. FIG. 16 is an explanatory view in case that an exposure operation on a white reticule is interrupted and an operation to replace the white reticule with a black reticule starts at the time point t1, at the time point t2, the delivery of the black reticule is completed and an exposure operation starts, at the time point t3, the exposure operation on the black reticule is interrupted and an operation for replacing the black reticule with the white reticule starts, and at the time point t4, the delivery of the white reticule ends and an exposure operation starts.

As the laser light irradiation is interrupted at the time point t1, the self-cleaning of the projection optical system 23 and the illumination optical system is interrupted as well. As a result, suspended contaminants

within the projection optical system 23 and the illumination optical system become re-adhered to the surfaces of the optical elements in the optical systems or the transmittances (of the optical materials) of the optical elements themselves fluctuate to result in a reduction in the transmittances of the projection optical system 23 and the illumination optical system. When the laser light irradiation is resumed at the time point  $t_2$ , self-cleaning of the optical elements starts again to result in an increase in the transmittances.

Thus, as explained earlier, at the time point  $t_2$  at which the laser light irradiation is resumed, the illuminance sensor 28 is moved onto the optical axis of the projection optical system 23 to measure the illuminance of the exposing light at the wafer stage 27 and, at the same time, the illuminance of the exposing light at the illumination optical system is detected by the integrator sensor 10. The transmittance at the time point  $t_2$  is calculated based upon the results of the measurement at the two sensors, and a time point  $t_0$  that corresponds to the calculated transmittance is determined based upon the time-varying transmittance characteristics of the black reticule represented by the dotted line. Then, when the exposure is resumed, the timer 58 that measures the length of exposure time elapsing after the

exposure start is reset at the time point  $t_0$ .

Consequently, when the exposure operation starts, the storage device 57 references the table storing the time-varying transmittance characteristics of the black

5 reticule in FIG. 16 to calculate the gain  $\beta$  by reading out the data corresponding to the length of time counted on the timer 58.

When the operation to replace the black reticule with the white reticule starts at the time point  $t_3$  and

10 exposure using the white reticule starts at the time point  $t_4$ , the transmittance at the time point  $t_4$  is calculated in a similar manner. Then, the table storing the time-varying transmittance characteristics at the white reticule is referenced to ascertain a time point  $t_0'$  that  
15 corresponds to the transmittance and the timer 58 that measures the length of exposure time elapsing after the exposure start is reset at the time point  $t_0'$ .

Consequently, when the exposure operation starts, the storage device 57 references the table storing the time-  
20 varying transmittance characteristics of the white reticule in FIG. 16 to calculate the gain  $\beta$  by reading out the data corresponding to the length of time counted on the timer 58.

In FIGS. 15 and 16, the transmittance at the optical  
25 system at the point in time at which exposure that has

been temporarily interrupted is resumed is ascertained, a time point corresponding to this transmittance is identified based upon the time-varying transmittance characteristics and the time point at which the exposure is to be resumed is corrected to control the illuminance of light exposing the wafer at a target value at the time of exposure restart. However, idle emission of laser pulses may be implemented at the time of the exposure restart until the transmittance on a characteristics curve representing the time-varying transmittance characteristics that is stored in advance is achieved. In such a case, it is necessary to provide a means for light blocking to ensure that laser pulses do not enter the wafer. For instance, a shutter that opens / closes the optical path between the projection optical system 23 and the wafer 25 may be provided. The shutter may be any of various types of shutters including mechanical shutters and electrical shutters constituted by using liquid crystal.

In addition, in this embodiment, the transmittance is detected by the integrator sensor 10 and the illuminance sensor 28 every time a wafer is replaced. However, it has been learned that the reduction in the transmittance occurring during the replacement is attributable to the reduced transmittances at the optical elements (optical

materials) themselves to a greater degree than to the re-adhesion of suspended contaminants. Consequently, instead of measuring the transmittance as described above during a wafer replacement, the time-varying characteristics may be simply measured and stored in advance, so that the transmittance can be predicted (calculated) based upon the stored time-varying transmittance characteristics during a wafer replacement to adjust the intensity of the exposing light emitted by the light source 1.

In this case, since the reduction in the transmittances at the illumination optical system and the projection optical system are mainly attributable to reductions in the transmittances of the optical materials themselves, the transmittances at the two optical systems can be ascertained with a high degree of accuracy through prediction (calculation) described above alone, and an improvement in throughput can be achieved without compromising the control accuracy on the exposure dose at the wafer. However, if the control is to be implemented through the prediction alone, the control error may become large as time elapses.

In this type of projection exposure apparatus, twenty five wafers, for instance, are processed in a batch as one lot. Thus, every time the exposure of wafers in a lot ends or every time the reticule is replaced, the



transmittance is detected by the integrator sensor 10 and the illuminance sensor 28. Then, the gain  $\beta$  is calculated by using these measured values as initial values and also by referencing the table of the time-varying

5 characteristics to adjust the intensity of the exposing light emitted by the light source 1. In this case, the reduction in throughput can be minimized without lowering the control accuracy on the exposure dose.

An example in which reticules are classified  
10 according to the ratio of the pattern area against the reticule surface area is explained above. However, reticules may be classified from another viewpoint, i.e., various reticules including a phase-shift reticule and a halftone phase reticule, that are employed to improve the  
15 resolution of the transfer have different transmittances, and in correspondence, the different time-varying transmittance characteristics at the projection optical system as well. In this case, the illumination method, too, should be modified in correspondence to the reticule  
20 that is being used.

The intensity of the exposing light emitted by the light source 1 is adjusted by either predicting or measuring time-varying transmittance at the optical system ranging from the integrator sensor 10 to the wafer stage  
25 26 to control the accumulated light quantity (exposure

dose) of the plurality of pulse beams irradiated onto each point on the wafer at a correct value in the first and second embodiments explained above. However, in a scanning projection exposure apparatus (e.g., the scanning stepper disclosed in the US Patent No. 5,473,410) that uses a pulse beam, for instance, as exposing light, the number of pulse beams to be irradiated on a given point on the wafer through scanning exposure can be adjusted in correspondence to the transmittance predicted as described above or in correspondence to the intensity of the exposing light on the wafer ascertained based upon the transmittance. In other words, the exposure dose may be controlled at a correct value by adjusting at least one of: the width of the exposing light on the wafer along the scanning direction, the oscillation frequency at the light source 1 and the scanning speed at the wafer. In short, the exposure dose (exposure quantity) imparted to the wafer in the scanning exposure operation should be controlled at a correct value by adjusting at least one of: the intensity of the exposing light on the wafer, the width of the exposing light, the oscillation frequency and the scanning speed. At this time, the intensity of the exposing light on the wafer may be adjusted through adjustment of the light emission intensity at the light source 1 achieved by varying the voltage applied to the

light source 1, through ND filter switching achieved by rotating the turret plate TP in FIG. 1 or through the combination of the adjustment of the light emission intensity and the ND filter switching.

5           In the case of a scanning type projection exposure apparatus (scanning stepper) that uses continuous light as exposing light, the exposure dose may be controlled at a correct value by adjusting at least one of the light emission intensity at the light source, the transmittance  
10 (extinction rate) at the light quantity adjuster such as the turret plate TP in FIG. 1 or the like, the width of the exposing light on the wafer and the scanning speed of the wafer in correspondence to the predicted transmittance value or the intensity of the exposing light at the wafer.  
15 In addition, in a projection exposure apparatus (stepper) that uses pulse beams as exposing light and exposes a wafer using the image of a pattern at a reticule while allowing the reticule and the wafer to remain stationary, at least, either the intensity of the exposing light at  
20 the wafer (the light emission intensity at the pulsed light source) or the number of exposing pulse beams needs to be adjusted. In a stepper that uses continuous light for exposing light, at least, either the intensity of the exposing light on the wafer (the light emission intensity  
25 at the light source or the like) or the length of

irradiation time needs to be adjusted.

If fluctuations of the transmittances at the illumination optical system and the projection optical system during exposure cannot be disregarded, the  
5 adjustment described earlier (e.g., adjustment of the intensity of the exposing light on the wafer, or (adjustment of the number of pulses) etc., may be implemented during the exposure. In particular, in a scanning stepper using pulse beams, the number of exposing  
10 pulses may be determined by taking into further consideration the quantity of change (or the change rate) of the transmittance occurring during scanning exposure.

The projection optical system 23 in the embodiments explained above (see FIG. 1) is constituted of only  
15 refractive optical elements such as lenses. However, the projection optical system may be a so-called catadioptric optical system achieved by combining reflective optical elements such as mirrors and refractive optical elements, or it may be constituted of reflective optical elements  
20 only.

In addition, while the explanation is given above on an example in which the exposing light is ArF laser, the present invention may be adopted in a projection exposure apparatus that uses EUVL such as soft x-rays with an even  
25 smaller wavelength. Furthermore, while a predictive line

of time-varying changes in the transmittance is calculated by measuring the transmittance of the exposing light at the optical system at a plurality of time points, another light source that emits light having a wavelength almost equal to the wavelength of the exposure light may be used instead. Moreover, if there is no fluctuation or very little fluctuation in the transmittance at the projection optical system, the time-varying transmittance characteristics need to be ascertained only for the illumination optical system. In this case, the transmittance should be measured based upon the output values from the integrator sensor 10 and the illuminance sensor which is placed on the reticule stage. If, on the other hand, there is no fluctuation or very little fluctuation in the transmittance at the illumination optical system, time-varying transmittance characteristics need only be ascertained for the projection optical system. In this case, the illuminance should be measured by extracting the exposing light in the area between the illumination optical system and the projection optical system. The exposing light itself may be used or another, separate light source that emits light having a wavelength almost equal to the wavelength of the exposing light may be employed, to determine the time-varying characteristics of transmittance at either the projection optical system

or the illumination optical system.

It is to be noted that an exposure apparatus that predicts time-varying transmittance characteristics to implement exposure control based upon the predicted characteristics or an exposure apparatus that implements exposure control based upon pre-stored time-varying transmittance characteristics is assembled by electrically, mechanically or chemically linking a great number of components explained in reference to the embodiments.

In more specific terms, the exposure apparatus in the embodiments can be fabricated by performing optical adjustment with the illumination optical system and the projection optical system each constituted of a plurality of lenses mounted at the main unit of the exposure apparatus, connecting wirings and pipings with the reticule stage and wafer stage constituted of a great number of mechanical parts at the main unit of the exposure apparatus and performing overall adjustment (electrical adjustment, operational verification and the like). It is to be noted that it is desirable to fabricate the exposure apparatus in a clean room in which the temperature and the degree of contamination are closely controlled.

The exposure apparatus does not need to be employed only for semiconductor production, and the present

invention may be adopted in a wide range of applications including an exposure apparatus for liquid crystal device that exposes a liquid crystal display element pattern onto a rectangular glass plate and an exposure apparatus  
5 employed to manufacture a thin film magnetic head. In addition, the magnifying power of the projection optical system may be the enlargement type, the reduction type or the neutral type.

Furthermore, the semiconductor device is fabricated  
10 through a step in which functions and performance of the device are designed, a step in which a reticule corresponding to the design is prepared, a step in which a wafer is produced from silicon material, a step in which a reticule pattern is exposed on the wafer by employing the  
15 exposure apparatus in the embodiments explained earlier, a step in which the device is assembled (includes dicing, bonding and packaging), an inspection step and the like.

What is claimed is;

1. A projection exposure method implemented in a projection exposure apparatus having an optical system that projects an image of a pattern illuminated by exposing light emitted by an exposing light source onto a photosensitive substrate with transmittance of the exposing light at said optical system changing over time, wherein:

transmittance of light having a wavelength substantially equal to the wavelength of the exposing light at said optical system is measured a plurality of time points; and

time-varying transmittance characteristics of said optical system are predicted based upon the plurality of transmittances thus measured, to project an image of the pattern onto the photosensitive substrate based upon the results of the prediction.

2. A projection exposure method according to claim 1, wherein:

the light having a wavelength substantially equal to the wavelength of the exposing light is exposing light emitted by said exposing light source.

3. A projection exposure method according to claim 1,



wherein:

said plurality of time points at which transmittance is measured constitute a time point before the light having substantially the same wavelength as that of the exposing light is irradiated on said optical system and a time point after the light having substantially the same wavelength as that of the exposing light is irradiated on said optical system over a specific length of time, and the two time points occur before the image of the pattern is projected onto the photosensitive substrate.

4. A projection exposure method according to claim 1, wherein:

said plurality of time points constitute a time point before the image of the pattern illuminated by the exposing light is projected onto the photosensitive substrate and a time point after the image of the pattern illuminated by the exposing light is projected onto the photosensitive substrate.

5. A projection exposure method according to claim 2, wherein:

said plurality of time points constitute a time point before the image of the pattern illuminated by the exposing light is projected onto a single photosensitive

substrate and a time point after the image of the pattern illuminated by the exposing light is projected onto the single photosensitive substrate.

5 6. A projection exposure method according to claim 2, wherein:

said plurality of time points constitute a time point before the image of the pattern illuminated by the exposing light is projected onto a specific area on the  
10 photosensitive substrate and a time point after the image of the pattern illuminated by the exposing light is projected onto said specific area.

7. A projection exposure method according to claim 6,  
15 wherein:

said specific area is an exposure area corresponding to one chip.

8. A projection exposure method according to claim 6,  
20 wherein:

said specific area is an exposure area corresponding to one shot.

9. A projection exposure method according to claim 2,  
25 wherein:

said optical system comprises an illumination optical system that illuminates the pattern with the exposing light and a projection optical system that projects the image of the pattern illuminated by said illumination optical system onto the photosensitive substrate; and

transmittance is measured a plurality of times at, at least, either said illumination optical system or said projection optical system, and time-varying transmittance characteristics at, at least, either said illumination optical system or said projection optical system are predicted.

10. A projection exposure method according to claim 1, wherein:

said optical system comprises an illumination optical system that illuminates the pattern with the exposing light; and

when fluctuations of transmittance at said illumination optical system result in fluctuations in transmittance at said optical system, transmittance of light having a wavelength substantially equal to the wavelength of the exposing light is measured at said illumination optical system at a plurality of time points to predict time-varying transmittance characteristics at said optical system.

11. A projection exposure method according to claim 10,  
wherein:

said optical system further comprises a projection  
5 optical system that projects the image of the pattern  
illuminated by said illumination optical system onto the  
photosensitive substrate and;

when fluctuations of transmittances at said  
illumination optical system and said projection optical  
10 system result in fluctuations of transmittance at said  
optical system, transmittances of light having a  
wavelength substantially equal to the wavelength of the  
exposing light are measured at said illumination optical  
system and said projection optical system at a plurality  
15 of time points to predict time-varying transmittance  
characteristics at said optical system.

12. A projection exposure method according to claim 1,  
wherein:

20 said optical system comprises a projection optical  
system that projects the image of the pattern onto the  
photosensitive substrate with the exposing light; and

when fluctuations of transmittance at said projection  
optical system result in fluctuations in transmittance at  
25 said optical system, transmittance of light having a

wavelength substantially equal to the wavelength of the exposing light is measured at said projection optical system at a plurality of time points to predict time-varying transmittance characteristics at said optical system.

13. A projection exposure method according to claim 12, wherein:

said optical system further comprises an illumination optical system that illuminates the pattern with the exposing light; and

when fluctuations of transmittances of light having a wavelength substantially equal to the wavelength of the exposing light at said illumination optical system and said projection optical system result in fluctuations of transmittance at said optical system, transmittances at said illumination optical system and said projection optical system are measured at a plurality of time points to predict time-varying transmittance characteristics at said optical system.

14. A projection exposure method according to claim 1, wherein:

an accumulated light quantity of the exposing light irradiated onto the photosensitive substrate is adjusted

to a correct value that corresponds to the sensitivity of the photosensitive substrate based upon said predicted time-varying transmittance characteristics.

5 15. A projection exposure method according to claim 1, wherein:

intensity of the exposing light irradiated onto the photosensitive substrate is adjusted based upon predicted time-varying transmittance characteristics.

10

16. A projection exposure method according to claim 1, wherein:

when the photosensitive substrate is made to move relative to the exposing light from the mask to pass  
15 through said projection optical system in synchronization with movement of the mask relative to the exposing light during a process of irradiating a pulse beam exposure light from said exposing light source and projecting the pattern formed on the mask onto the photosensitive  
20 substrate;

an accumulated light quantity of the exposing light is controlled at a correct value corresponding to the sensitivity of the photosensitive substrate by adjusting at least one of: the intensity of the exposing light  
25 entering the photosensitive substrate, the width of the

exposing light on the photosensitive substrate relative to the traveling direction in which the photosensitive substrate moves, the traveling speed of the photosensitive substrate moving relative to the traveling direction and  
5 the oscillation frequency of said exposing light source, based upon the time-varying transmittance characteristics.

17. A projection exposure method according to claim 2, wherein:

10 time-varying transmittance characteristics are calculated using a plurality of transmittances, each calculated based upon a ratio of an illuminance of the exposing light emitted by said exposing light source and an illuminance of the exposing light on the photosensitive  
15 substrate.

18. A projection exposure apparatus having an optical system that projects an image of a pattern illuminated by exposing light emitted by an exposing light source onto a  
20 photosensitive substrate with transmittance of the exposing light at said optical system changing over time, comprising:

a measuring device that measures transmittance of light having a wavelength substantially equal to the  
25 wavelength of the exposing light at said optical system at

a plurality of time points; and

a prediction device that predicts time-varying transmittance characteristics at said optical system based upon a plurality of measured transmittances.

5

19. A projection exposure apparatus according to claim 18, wherein:

the light having a wavelength substantially equal to the wavelength of the exposing light is exposing light  
10 emitted by said exposing light source.

20. A projection exposure apparatus according to claim 18, wherein:

said plurality of time points at which transmittance  
15 is measured constitute a time point before the light having substantially the same wavelength as that of the exposing light is irradiated on said optical system and a time point after the light having substantially the same wavelength as that of the exposing light is irradiated on  
20 said optical system over a specific length of time, and the two time points occur before the image of the pattern is projected onto the photosensitive substrate.

21. A projection exposure apparatus according to claim 19,  
25 wherein:



said plurality of time points constitute a time point before the image of the pattern illuminated by the exposing light is projected onto the photosensitive substrate and a time point after the image of the pattern illuminated by the exposing light is projected onto the photosensitive substrate.

22. A projection exposure apparatus according to claim 19, wherein:

10       said plurality of time points constitute a time point before the image of the pattern illuminated by the exposing light is projected onto a single photosensitive substrate and a time point after the image of the pattern illuminated by the exposing light is projected onto the single photosensitive substrate.

23. A projection exposure apparatus according to claim 19, wherein:

20       said plurality of time points constitute a time point before the image of a pattern illuminated by the exposing light is projected onto a specific area on the photosensitive substrate and a time point after the image of the pattern illuminated by the exposing light is projected onto said specific area.

24. A projection exposure apparatus according to claim 23,  
wherein:

said specific area is an exposure area corresponding  
to one chip.

5

25. A projection exposure apparatus according to claim 23,  
wherein:

said specific area is an exposure area corresponding  
to one shot.

10

26. A projection exposure apparatus according to claim 19,  
wherein:

said optical system comprises an illumination optical  
system that illuminates the pattern with the exposing  
light and a projection optical system that projects the  
image of the pattern illuminated by said illumination  
optical system onto the photosensitive substrate; and

15

said measuring device performs measurement of the  
transmittance a plurality of times at, at least, either  
said illumination optical system or said projection  
optical system and said prediction device predicts time-  
varying transmittance characteristics at, at least, either  
said illumination optical system or said projection  
optical system.

20

25

27. A projection exposure apparatus according to claim 19,  
wherein:

said optical system comprises an illumination optical  
system that illuminates the pattern with the exposing

5 light; and

when fluctuations of transmittance at said  
illumination optical system result in fluctuations in  
transmittance at said optical system,

said measuring device measures transmittance of the  
10 light having a wavelength substantially equal to the  
wavelength of the exposing light at said illumination  
optical system at a plurality of time points and said  
prediction device predicts time-varying transmittance  
characteristics at said optical system based upon the  
15 result of measurement performed a plurality of times.

28. A projection exposure apparatus according to claim 27,  
wherein:

said optical system further comprises a projection  
20 optical system that projects the image of the pattern  
illuminated by said illumination optical system onto the  
photosensitive substrate and;

when fluctuations of transmittances at said  
illumination optical system and said projection optical  
25 system result in fluctuations of transmittance at said

optical system, transmittances of the light having a wavelength substantially equal to the wavelength of the exposing light at said illumination optical system and said projection optical system are measured at a plurality of time points and said prediction device predicts time-varying transmittance characteristics at said optical system based upon results of measurement performed a plurality of times.

29. A projection exposure apparatus according to claim 18, wherein:

said optical system comprises a projection optical system that projects the image of the pattern onto the photosensitive substrate with the exposing light; and

when fluctuations of transmittance at said projection optical system result in fluctuations in transmittance at said optical system,

said measuring device measures the transmittance of the light having a wavelength substantially equal to the wavelength of the exposing light at said projection optical system at a plurality of time points and said prediction device predicts time-varying transmittance characteristics at said optical system.

30. A projection exposure apparatus according to claim 29,

wherein:

said optical system further comprises an illumination optical system that illuminates the pattern with the exposing light and;

5       when fluctuations of transmittances at said illumination optical system and said projection optical system result in fluctuations of transmittance at said optical system, transmittances at said illumination optical system and said projection optical system are  
10       measured at a plurality of time points and said prediction device predicts time-varying transmittance characteristics at said optical system based upon results of measurements performed a plurality of times.

15       31. A projection exposure apparatus according to claim 18, further comprising:

an accumulated exposure quantity controller that controls an accumulated light quantity of the exposing light irradiated onto the photosensitive substrate at a  
20       correct value corresponding to sensitivity of the photosensitive substrate, based upon the predicted time-varying transmittance characteristics.

32. A projection exposure apparatus according to claim 18,  
25       further comprising:

an exposing light intensity adjuster that adjusts intensity of the exposing light irradiated onto the photosensitive substrate based upon the predicted time-varying transmittance characteristics.

5

33. A projection exposure apparatus according to claim 18, wherein:

when the photosensitive substrate is made to move relative to the exposing light from the mask to pass  
10 through said projection optical system in synchronization with movement of the mask relative to the exposing light during a process of irradiating a pulse beam exposure light from said exposing light source and projecting a pattern formed on the mask onto the photosensitive  
15 substrate;

said projection exposure apparatus comprises a control device that controls the accumulated light quantity of the exposing light at a correct value corresponding to the sensitivity of the photosensitive  
20 substrate by adjusting at least one of: an intensity of the exposing light entering the photosensitive substrate, a width of the exposing light on the photosensitive substrate relative to the traveling direction in which the photosensitive substrate moves, a traveling speed of the  
25 photosensitive substrate moving relative to the traveling

direction and an oscillation frequency of said exposing light source, based upon the time-varying transmittance characteristics.

5 34. A projection exposure apparatus according to claim 19, wherein:

said prediction device calculates time-varying transmittance characteristics based upon a plurality of transmittances each calculated in correspondence to a  
10 ratio of an illuminance of the exposing light emitted by said exposing light source and an illuminance of the exposing light on the photosensitive substrate.

35. A method of fabricating a semiconductor device by  
15 using a projection exposure apparatus having an optical system that projects the image of a pattern illuminated by exposing light emitted from an exposing light source onto a photosensitive substrate with transmittance of the exposing light at said optical system changing over time,  
20 wherein:

transmittance of light having a wavelength that is substantially equal to the wavelength of the exposing light at said optical system is measured at a plurality of time points;

25 time-varying transmittance characteristics at said

optical system are predicted based upon the plurality of measured transmittances; and

the image of the pattern is projected onto the photosensitive substrate based upon the results of the  
5 prediction.

36. An optical cleaning method for optically cleaning an optical system in a projection exposure apparatus that projects the image of a pattern illuminated by exposing  
10 light emitted from an exposing light source onto a photosensitive substrate with transmittance of the exposing light at said optical system changing over time, wherein:

transmittance of light having a wavelength  
15 substantially equal to the wavelength of the exposing light at said optical system is measured at a plurality of time points; and

said optical system is optically cleaned while predicting the time-varying transmittance characteristics  
20 at said optical system based upon the plurality of measured transmittances.

37. An optical cleaning method according to claim 36, wherein:

25 said plurality of time points at which transmittance



is measured constitute a time point before the light having substantially the same wavelength as that of the exposing light is irradiated on said optical system and a time point after the light having substantially the same wavelength as that of the exposing light is irradiated on said optical system over a specific length of time, and the two time points occur before the image of the pattern is projected onto the photosensitive substrate.

38. A projection exposure apparatus comprising an illumination optical system that illuminates a mask at which a specific pattern is formed with exposing light emitted by an exposing light source, and a projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive substrate with transmittance of the exposing light at said projection optical system changing over time, further comprising:

a mask illuminance detector that detects the illuminance of the exposing light irradiated on the mask from an exposing light source;

a substrate illuminance detector that detects the illuminance of the exposing light on the photosensitive substrate;

a prediction device that predicts time-varying

transmittance characteristics of the exposing light at said projection optical system by calculating the ratio of the illuminance of the exposing light irradiated on the mask detected by said mask illuminance detector and the illuminance of the exposing light irradiated on the substrate detected by said substrate illuminance detector a plurality of times; and

a control device that adjusts the accumulated light quantity of the exposing light entering the photosensitive substrate based upon the predicted time-varying characteristics and the ratio of the two illuminances.

39. A projection exposure apparatus according to claim 38, wherein:

when transmittance of the exposing light at said illumination optical system, too, changes over time,

said prediction device predicts of time-varying transmittance characteristics of the exposing light at the entire optical system comprising said illumination optical system and said projection optical system.

40. A projection exposure apparatus comprising an illumination optical system that illuminates a mask at which a specific pattern is formed with exposing light emitted by an exposing pulsed light source, and a

projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive substrate with transmittance of the exposing light at, at least, either  
5 said illumination optical system or said projection optical system changing over time, further comprising:

a mask illuminance detector that detects the illuminance of the exposing light irradiated on the mask from said exposing pulsed light source;

10 a substrate illuminance detector that detects the illuminance of the exposing light on the photosensitive substrate;

a prediction device that predicts time-varying transmittance characteristics of the exposing light at  
15 said projection optical system by calculating the ratio of the illuminance of the exposing light irradiated on the mask detected by said mask illuminance detector and the illuminance of the exposing light irradiated on the substrate detected by said substrate illuminance detector  
20 a plurality of times; and

a control device that adjusts, at least, either the intensity of pulsed exposing light irradiated onto the photosensitive substrate or the number of pulses to control an accumulated light quantity of the exposing  
25 light irradiated onto the photosensitive substrate at a

correct value corresponding to the sensitivity of the photosensitive substrate, based upon predicted time-varying characteristics and the ratio of the two illuminances.

5

41. A projection exposure method implemented in a projection exposure apparatus having an illumination optical system that illuminates a mask having a specific pattern formed therein with exposing light emitted by an exposure pulsed light source and a projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive substrate with transmittance of the exposing light at, at least, either said illumination optical system or said projection optical system changing over time, comprising:

a step in which time-varying transmittance characteristics of the exposing light at, at least, either said illumination optical system or said projection optical system are predicted by calculating the ratio of illuminance of the exposing light emitted by said exposing pulsed light source and an illuminance of the exposing light on the photosensitive substrate a plurality of times; and

25 a step in which, at least, either the intensity of

the pulsed exposing light entering the photosensitive substrate or the number of pulses is adjusted based upon the ratio of the illuminance of the exposing light emitted by said exposing pulsed light source and the illuminance  
5 of the exposing light on the photosensitive substrate and the predicted time-varying transmittance characteristics.

42. A projection exposure method implemented in a projection exposure apparatus having an illumination  
10 optical system that illuminates a mask having a specific pattern formed therein with exposing light emitted from an exposing light source and a projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive  
15 substrate with transmittance of the exposing light at, at least, either said illumination optical system or said projection optical system changing over time, comprising:

a step in which time-varying transmittance characteristics of the exposing light at, at least, either  
20 said illumination optical system or said projection optical system are predicted by calculating the ratio of illuminance of the exposing light emitted by said exposing light source and an illuminance of the exposing light on the photosensitive substrate a plurality of times; and  
25 a step in which, at least, the intensity of the

exposing light irradiated onto the photosensitive substrate is adjusted based upon the ratio of the illuminance of the exposing light emitted by said exposing light source and an illuminance of the exposing light on the photosensitive substrate and the predicted time-varying transmittance characteristics.

43. A projection exposure method implemented in a projection exposure apparatus having an illumination optical system that illuminates a mask having a specific pattern formed therein with exposing light emitted from an exposing light source and a projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive substrate with transmittance of the exposing light at said projection optical system changing over time, comprising:

a step in which time-varying transmittance characteristics of the exposing light at said projection optical system are predicted by calculating the ratio of illuminance of the exposing light emitted by said exposing light source and an illuminance of the exposing light on the photosensitive substrate a plurality of times; and

a step in which the intensity of the exposing light irradiated onto the photosensitive substrate is adjusted based upon the ratio of the illuminance of the exposing

light emitted by said exposing light source and an illuminance of the exposing light on the photosensitive substrate and the predicted time-varying transmittance characteristics.

5

44. An exposure method implemented in a projection exposure apparatus having an illumination optical system that illuminates a mask having a specific pattern formed therein with exposing light emitted from an exposing light source and a projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive substrate with transmittance of the exposing light at, at least, either said illumination optical system or said projection optical system changing over time, wherein:

the intensity of the exposing light irradiated onto the photosensitive substrate is adjusted based upon a ratio of an illuminance of the exposing light emitted by said exposing light source and illuminance of the exposing light on the photosensitive substrate and time-varying transmittance characteristics of the exposing light at, at least, either said illumination optical system or said projection optical system.

25 45. A projection exposure method implemented in a

projection exposure apparatus having an illumination optical system that illuminates a mask having a specific pattern formed therein with exposing light emitted from an exposing light source and a projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive substrate with transmittance of the exposing light at said projection optical system changing over time, wherein:

an accumulated quantity of the exposing light entering the photosensitive substrate is adjusted based upon the ratio of an illuminance of the exposing light emitted by said exposing light source and an illuminance of the exposing light on the photosensitive substrate and time-varying transmittance characteristics of the exposing light at said projection optical system.

46. An exposure method according to claim 45, wherein:

when transmittance of the exposing light at said illumination optical system, too, changes over time, the intensity of the exposing light emitted by said exposing light source is adjusted based upon time-varying transmittance characteristics of the exposing light at the entire optical system comprising said illumination optical system and said projection optical system, and a ratio of the illuminances.



47. An exposure method according to claim 45, wherein:

the exposing light is a pulse beam and the accumulated light quantity of the exposing light is controlled at a correct value corresponding to the sensitivity of the photosensitive substrate by adjusting at least, either the intensity of the exposing light entering the photosensitive substrate or the number of the exposing light beams irradiated on a given point on the photosensitive substrate.

48. An exposure method according to claim 45, wherein:

the photosensitive substrate is caused to move relative to the exposing light from the mask and passing through said projection optical system in synchronization with the movement of the mask relative to the exposing light, in order to transfer the pattern onto the photosensitive substrate.

49. An exposure method according to claim 48, wherein:

the exposing light is a pulse beam and the accumulated light quantity of the exposing light is controlled at a correct value corresponding to the sensitivity of the photosensitive substrate by adjusting at least one of: the intensity of the exposing light

entering the photosensitive substrate, the width of the exposing light on the photosensitive substrate relative to the direction in which the photosensitive substrate moves, the traveling speed of the photosensitive substrate  
5 relative to the traveling direction and an oscillation frequency of said exposing light source.

50. A projection exposure apparatus comprises an illumination optical system that illuminates a mask at  
10 which a specific pattern is formed with exposing light emitted by an exposing pulsed light source, and a projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive substrate with  
15 transmittance of the exposing light at, at least, either said illumination optical system or said projection optical system changing over time, further comprising:

a mask illuminance detector that detects the illuminance of the exposing light irradiated on the mask  
20 from said exposing light source;

a substrate illuminance detector that detects the illuminance of the exposing light on the photosensitive substrate;

a storage device that stores in memory  
25 characteristics of time-varying transmittance of the

exposing light at said projection optical system; and

a control device that adjusts the accumulated light quantity of the exposing light entering the photosensitive substrate based upon the ratio of illuminance of the exposing light irradiated on the mask detected by said mask illuminance detector and the illuminance of the exposing light irradiated onto the photosensitive substrate detected by said substrate illuminance detector and time-varying characteristics stored in said storage device.

51. A projection exposure apparatus according to claim 50, wherein:

when transmittance of the exposing light at said illumination optical system, too, changes over time, time-varying transmittance characteristics of the exposing light at the entire optical system comprising said illumination optical system and said projection optical system are stored in said storage device.

52. A projection exposure apparatus according to claim 50 or 51, wherein:

a plurality of sets of time-varying characteristics of the exposing light are set in correspondence to varying exposure conditions and stored in said storage device.

53. A projection exposure apparatus according to claim 52,  
wherein:

when an exposure condition does not fit any of the  
5 exposure conditions stored in said storage device, an  
interpolation operation of time-varying characteristics  
stored in memory is performed to calculate transmittance.

54. A projection exposure apparatus according to claim 52,  
10 wherein:

the exposure conditions are illuminating conditions  
at said illumination optical system.

55. A projection exposure apparatus according to claim 52,  
15 wherein:

the exposure conditions are types of the masks.

56. A projection exposure apparatus according to claim 52,  
wherein:

20 the exposure conditions are numerical apertures at  
said projection optical system.

57. An exposure method implemented in a projection  
exposure apparatus having an illumination optical system  
25 that illuminates a mask having a specific pattern formed

therein with exposing light emitted from an exposing light source and a projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive

5 substrate with transmittance of the exposing light at, at least, either said illumination optical system or said projection optical system changing over time, wherein:

at least, either the intensity of the pulsed exposing light entering the photosensitive substrate or the number  
10 of pulses is adjusted based upon the ratio of the illuminance of the exposing light emitted by said exposing light source and an illuminance of the exposing light on the photosensitive substrate and the predicted time-varying transmittance characteristics.

15

58. A projection exposure apparatus comprising an illumination optical system that illuminates a mask at which a specific pattern is formed with exposing light emitted by an exposing pulsed light source, and a

20 projection optical system that projects the image of the pattern at the mask illuminated by said illumination optical system onto a photosensitive substrate with transmittance of the exposing light at, at least, either said illumination optical system or said projection  
25 optical system changing over time, further comprising:

a mask illuminance detector that detects the illuminance of the exposing light irradiated on the mask from said exposing pulsed light source;

a substrate illuminance detector that detects the  
5 illuminance of the exposing light on the photosensitive substrate;

a storage device that stores in memory characteristics of time-varying transmittance of the exposing light at said projection optical system; and

10 a control device that adjusts, at least, either the intensity of the pulsed exposing light irradiated onto the photosensitive substrate or the number of pulses, to control the accumulated light quantity of the exposing light irradiated onto the photosensitive substrate at a  
15 correct value corresponding to the sensitivity of the photosensitive substrate based upon the ratio of illuminance of the exposing light irradiated on the mask detected by said mask illuminance detector and the illuminance of the exposing light irradiated on the  
20 photosensitive substrate detected by said substrate illuminance detector and time-varying transmittance characteristics stored in said storage device.

59. A projection exposure apparatus having an optical  
25 system that projects the image of a pattern illuminated by

exposing light emitted from an exposing light source onto the photosensitive substrate with transmittance of the exposing light at said optical system changing over time, comprising:

5           a measuring device that is provided at a position at which transmittance of said optical system can be measured and measures transmittance of light having a wavelength substantially equal to the wavelength of the exposing light at said optical system at a plurality of time  
10 points; and

          a prediction device that is connected to said measuring device and predicts time-varying transmittance characteristics at said optical system based upon a plurality of measured transmittances.

15

60. A projection exposure apparatus according to claim 59, wherein:

          said optical system comprises an illumination optical system that illuminates the pattern with the exposing  
20 light and a projection optical system that projects the image of the pattern illuminated by said illumination optical system onto the photosensitive substrate; and

          said measuring device comprises a pattern illuminance detector that detects an illuminance of the exposing light  
25 irradiated on the pattern from said exposing light source

and a substrate illuminance detector that detects an illuminance of the exposing light on the photosensitive substrate.

5 61. A method of assembling a projection exposure apparatus having an optical system that projects an image of a pattern illuminated by exposing light from an exposing light source onto a photosensitive substrate with transmittance of the exposing light at said optical system  
10 changing over time, wherein:

a measuring device that measures transmittance of light having a wavelength substantially equal to the wavelength of the exposing light at said optical system at a plurality of time points is provided at a position at  
15 which transmittance at said optical system can be measured; and

a prediction device that predicts time-varying transmittance characteristics at said optical system based upon a plurality of measured transmittances is connected  
20 to said measuring device.



FIG. 1

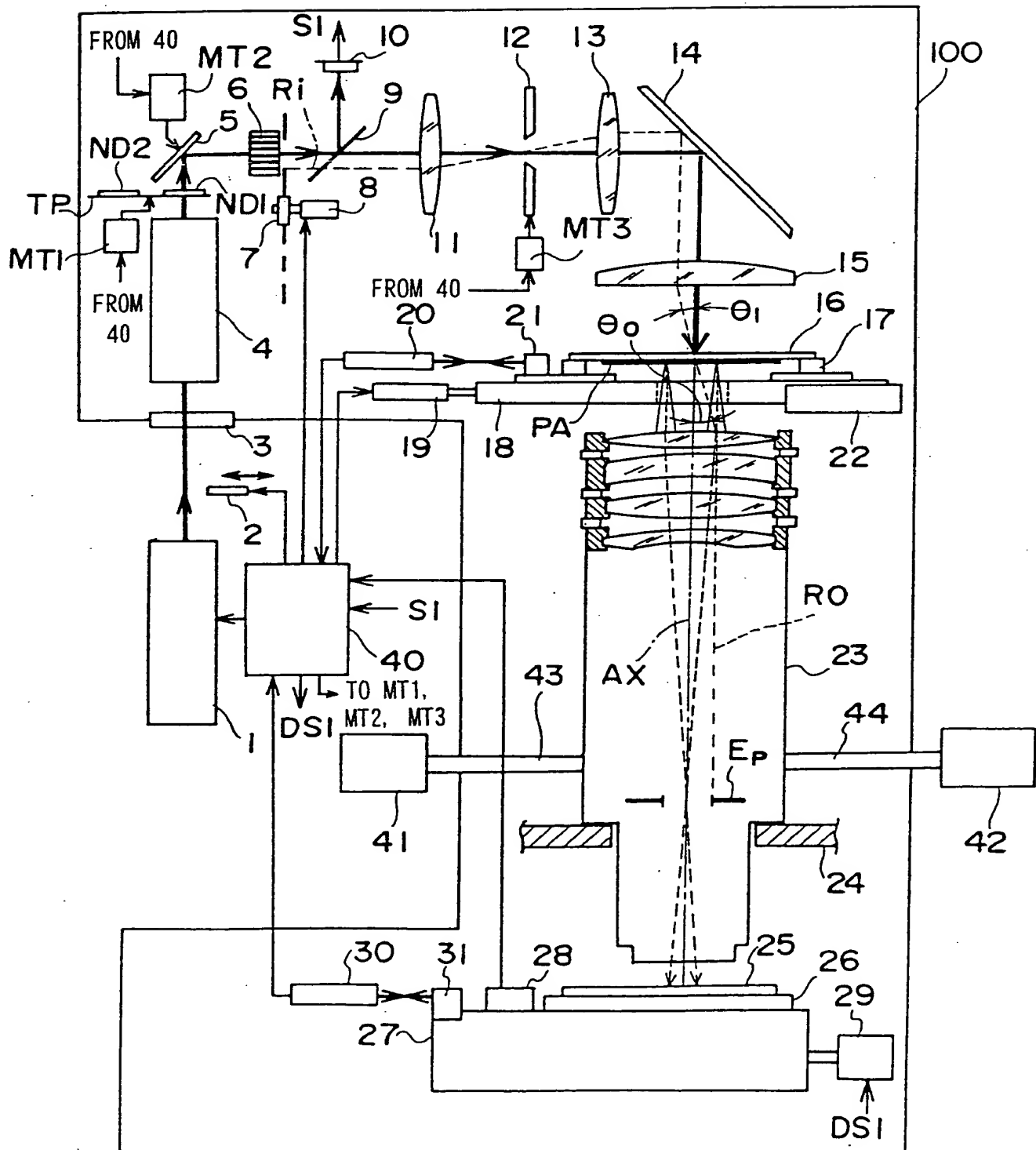


FIG. 2

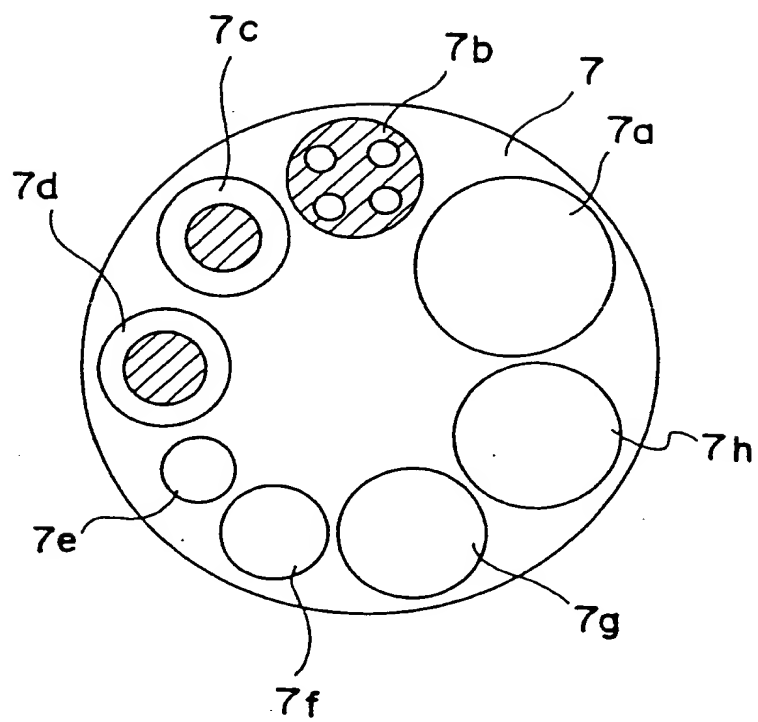


FIG. 3

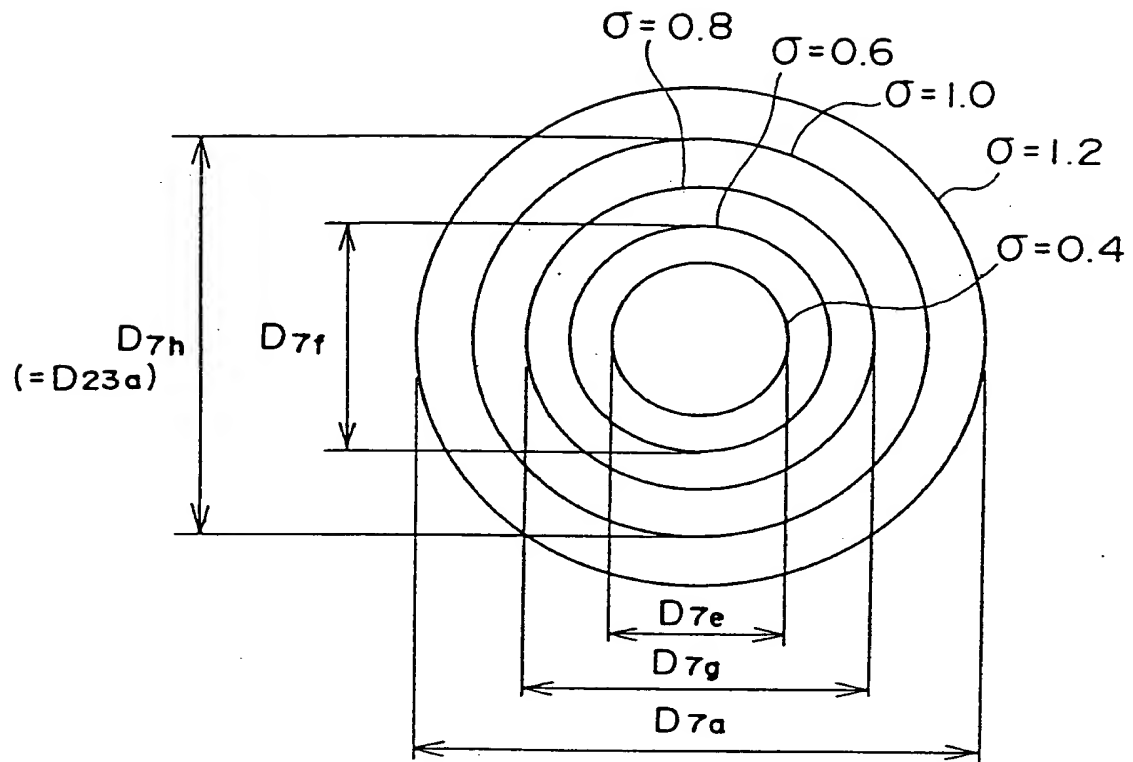


FIG. 4

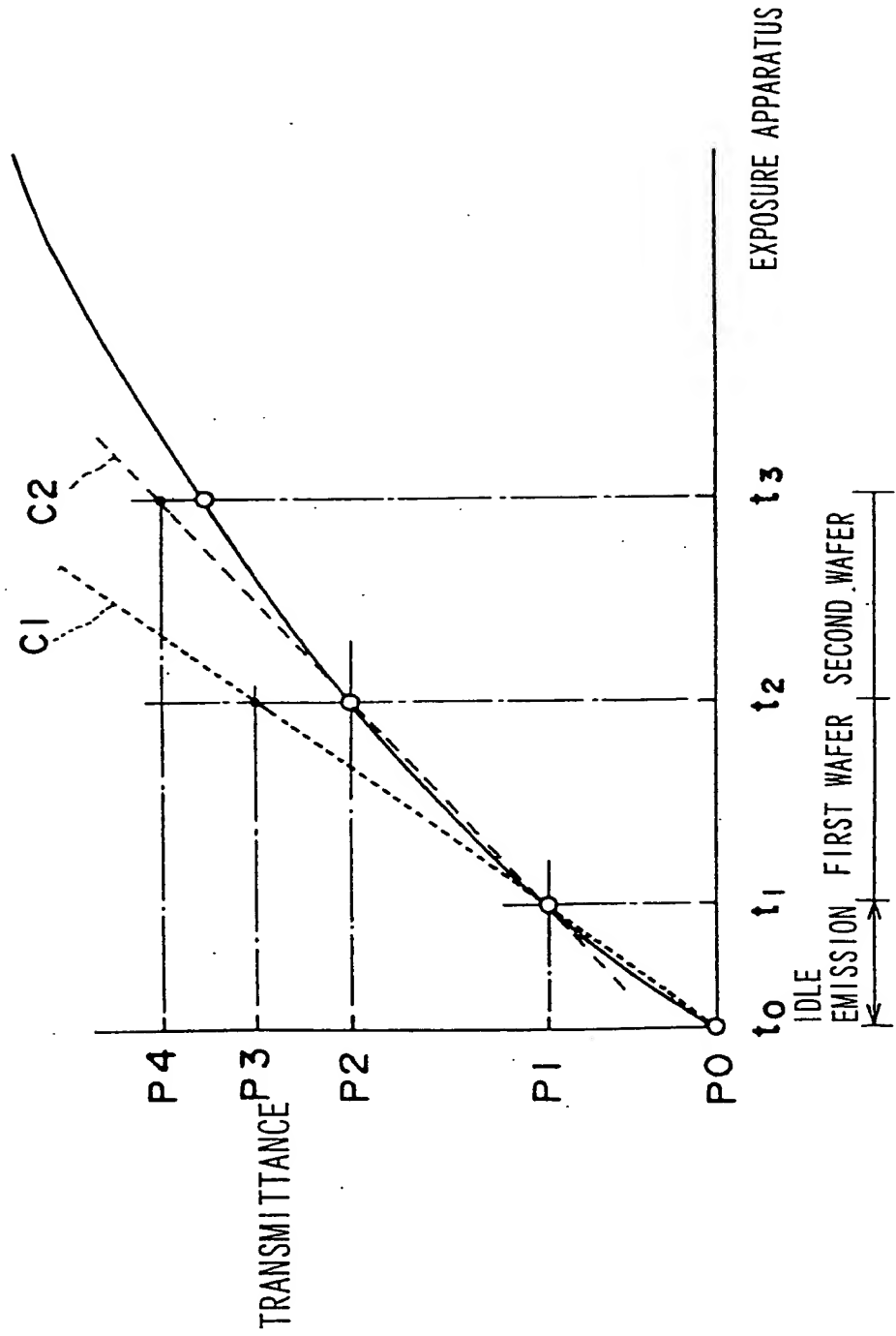


FIG. 5

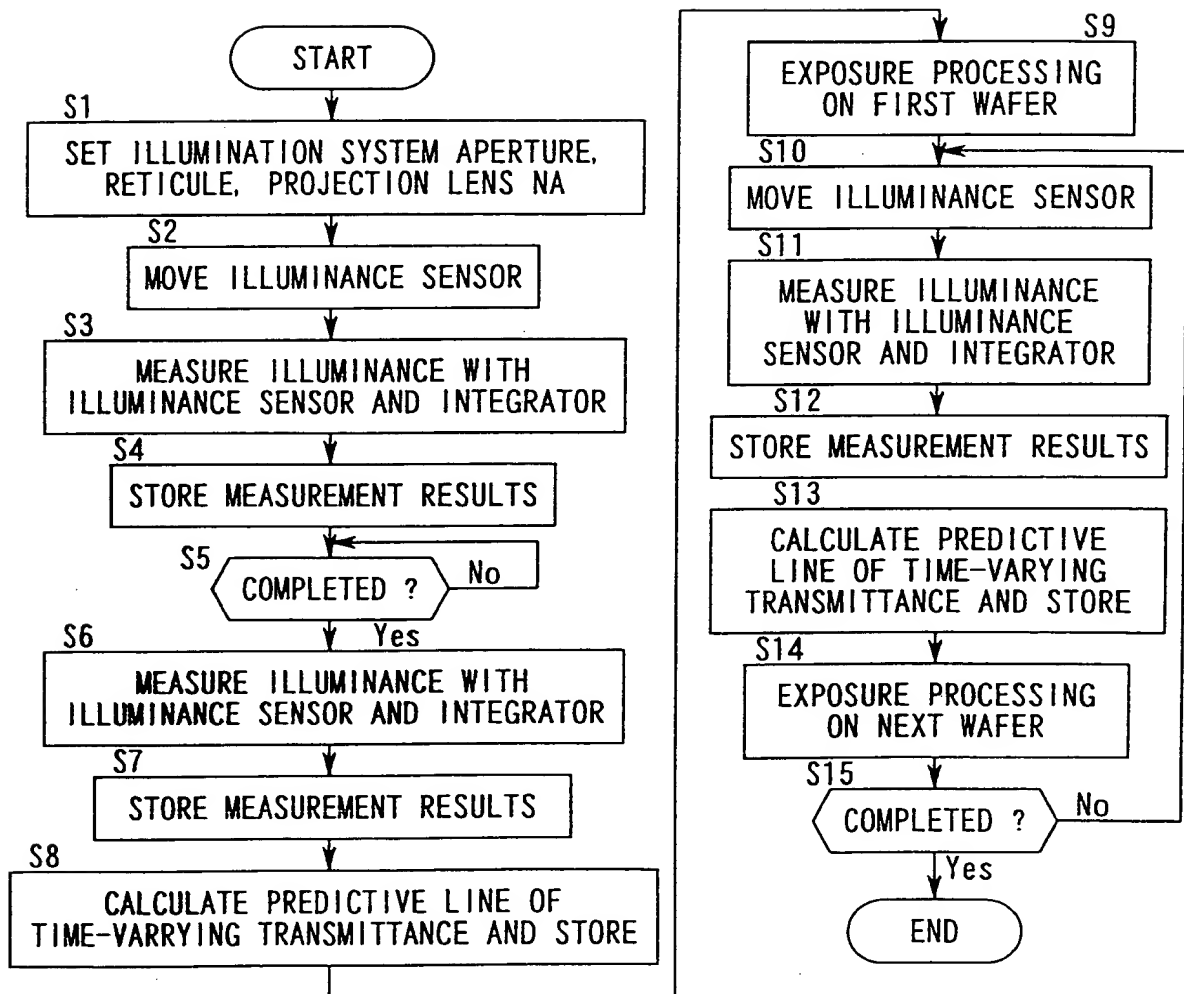


FIG. 6

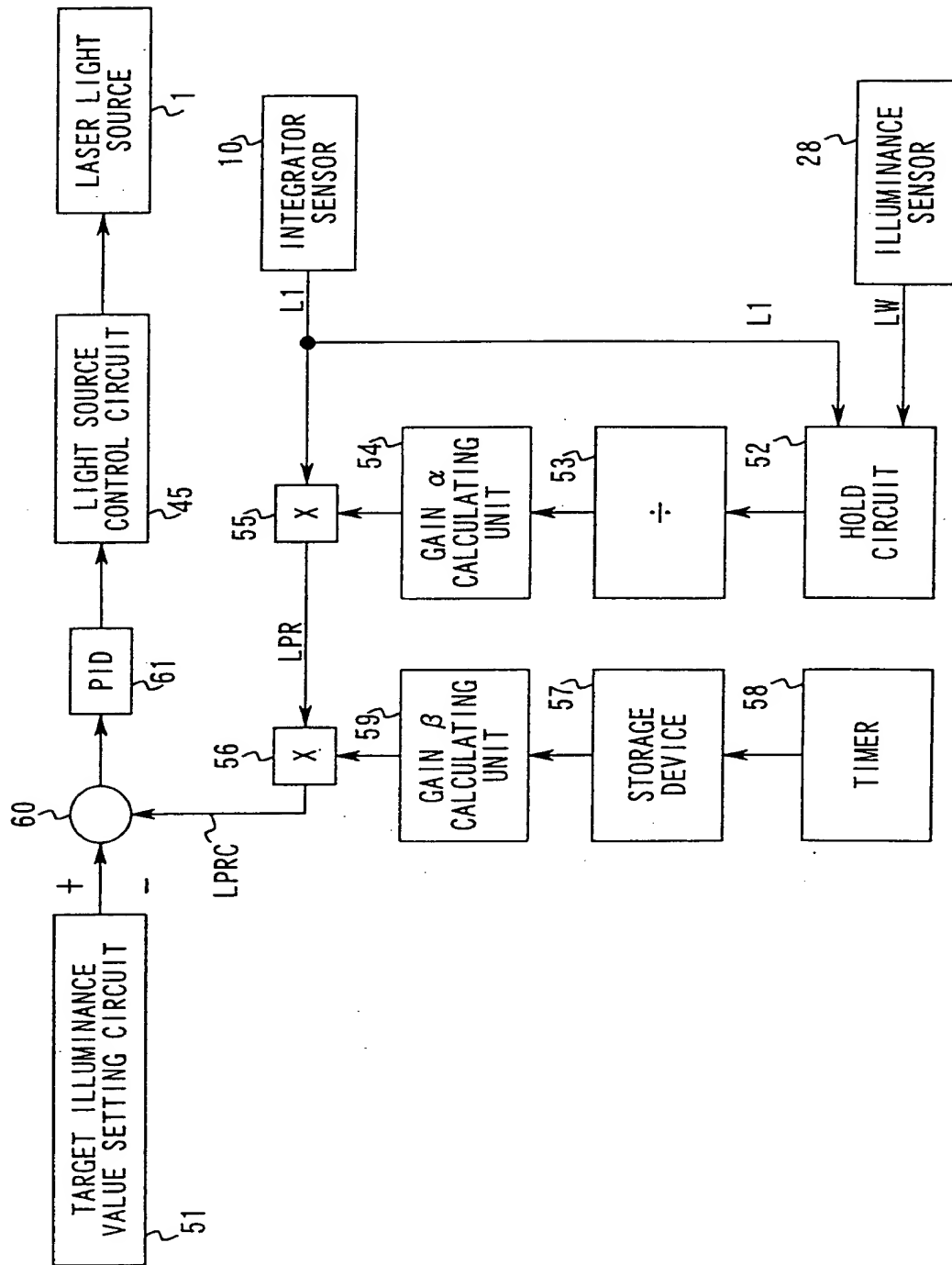


FIG. 7

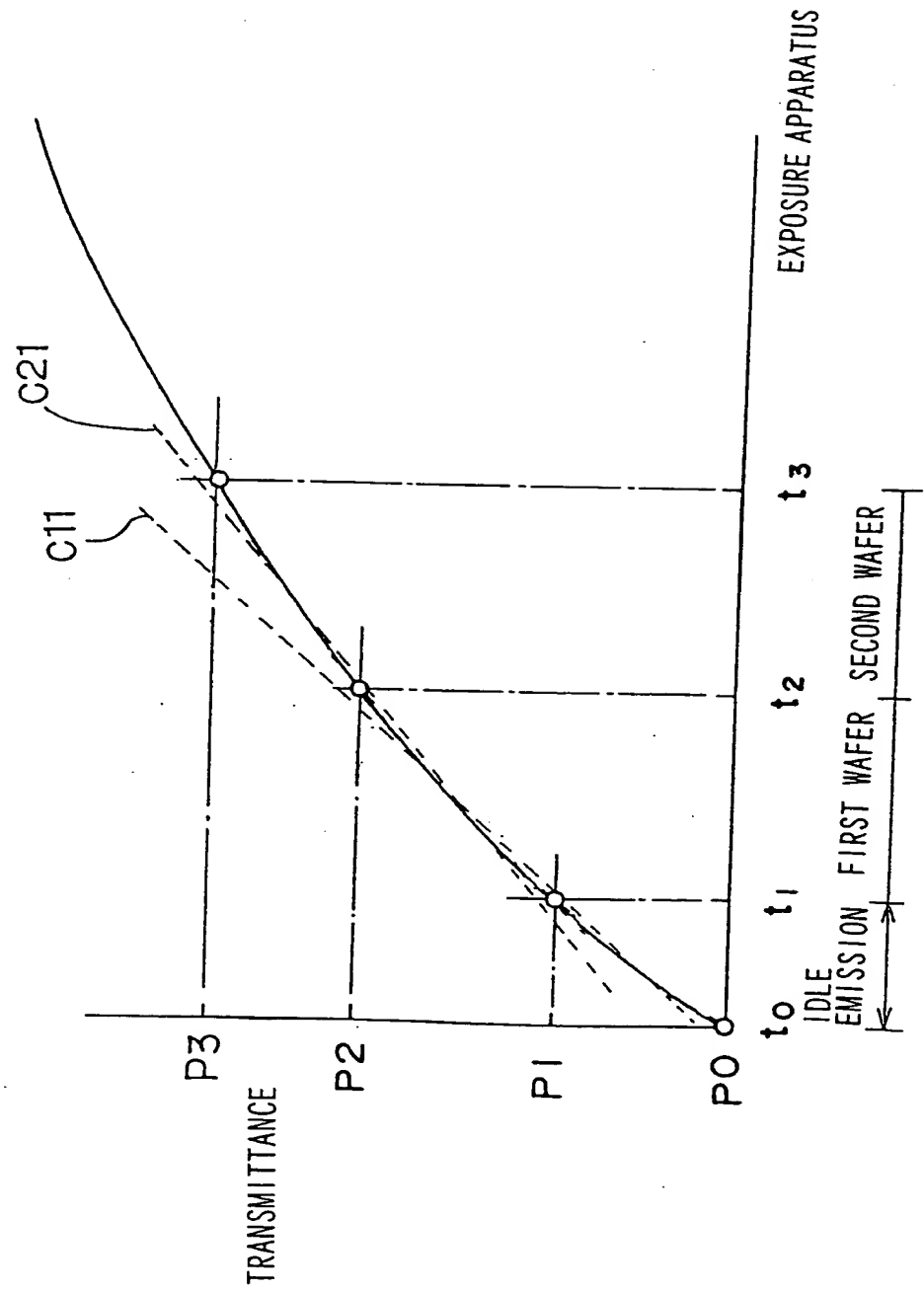


FIG. 8

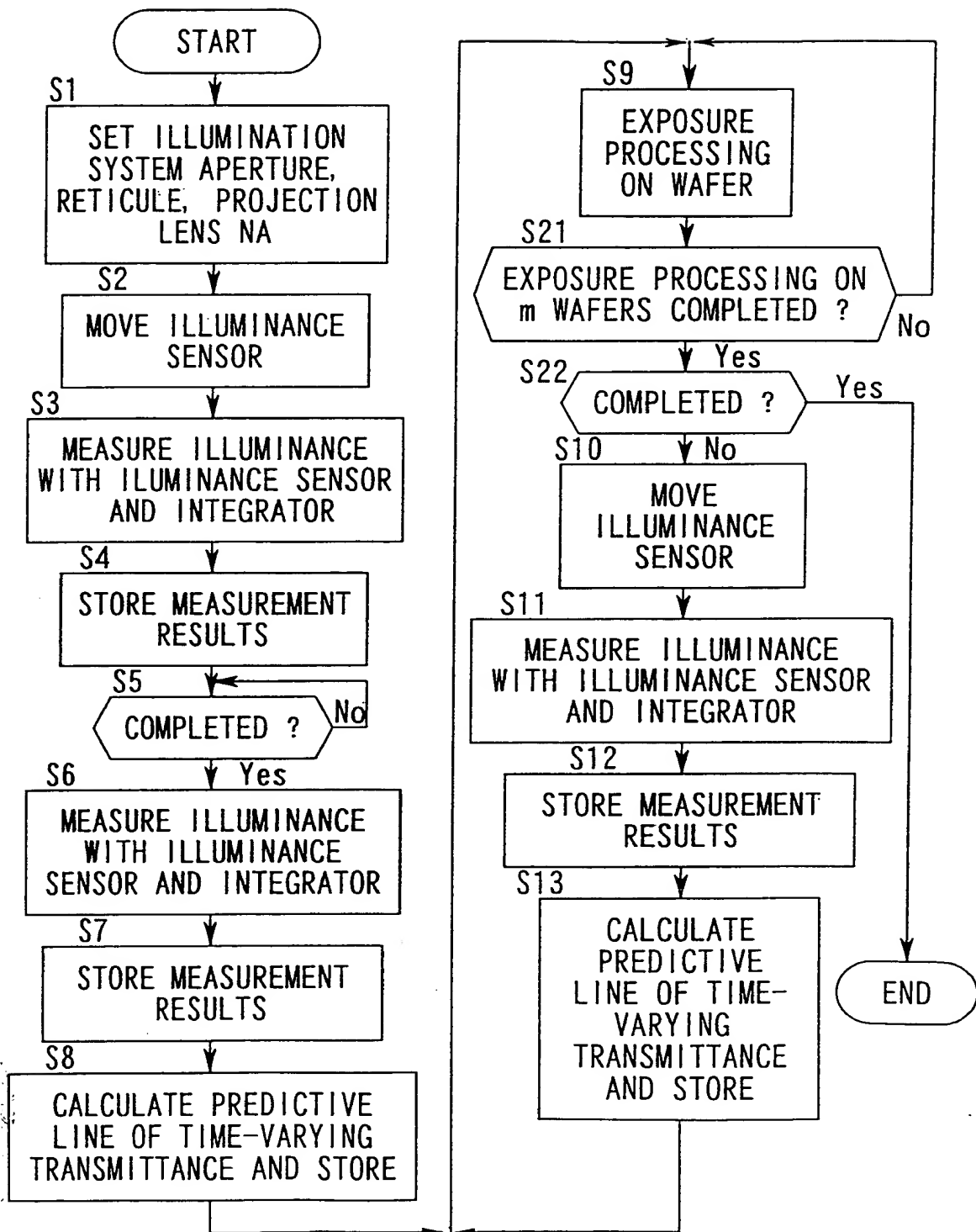




FIG. 9

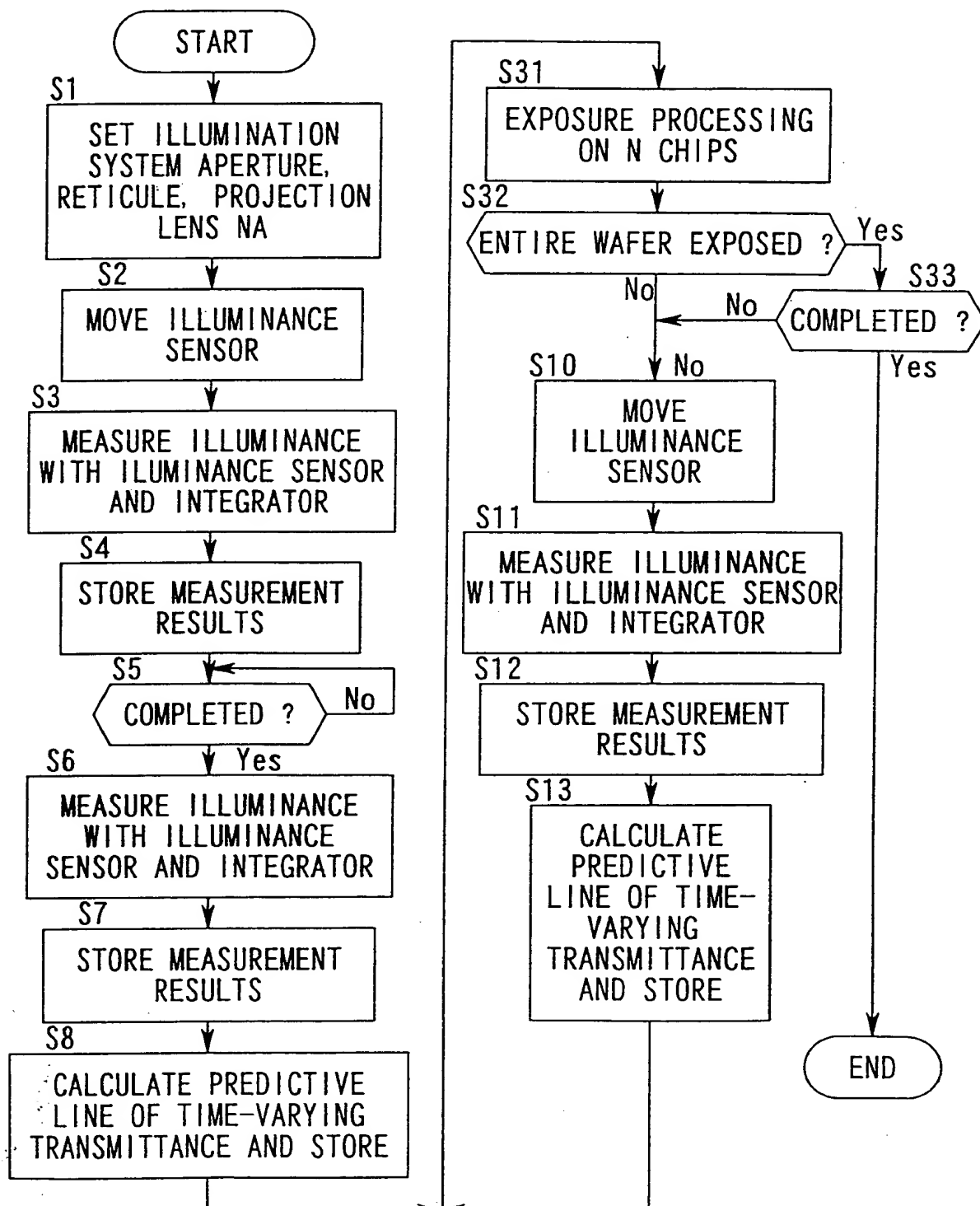


FIG. 10

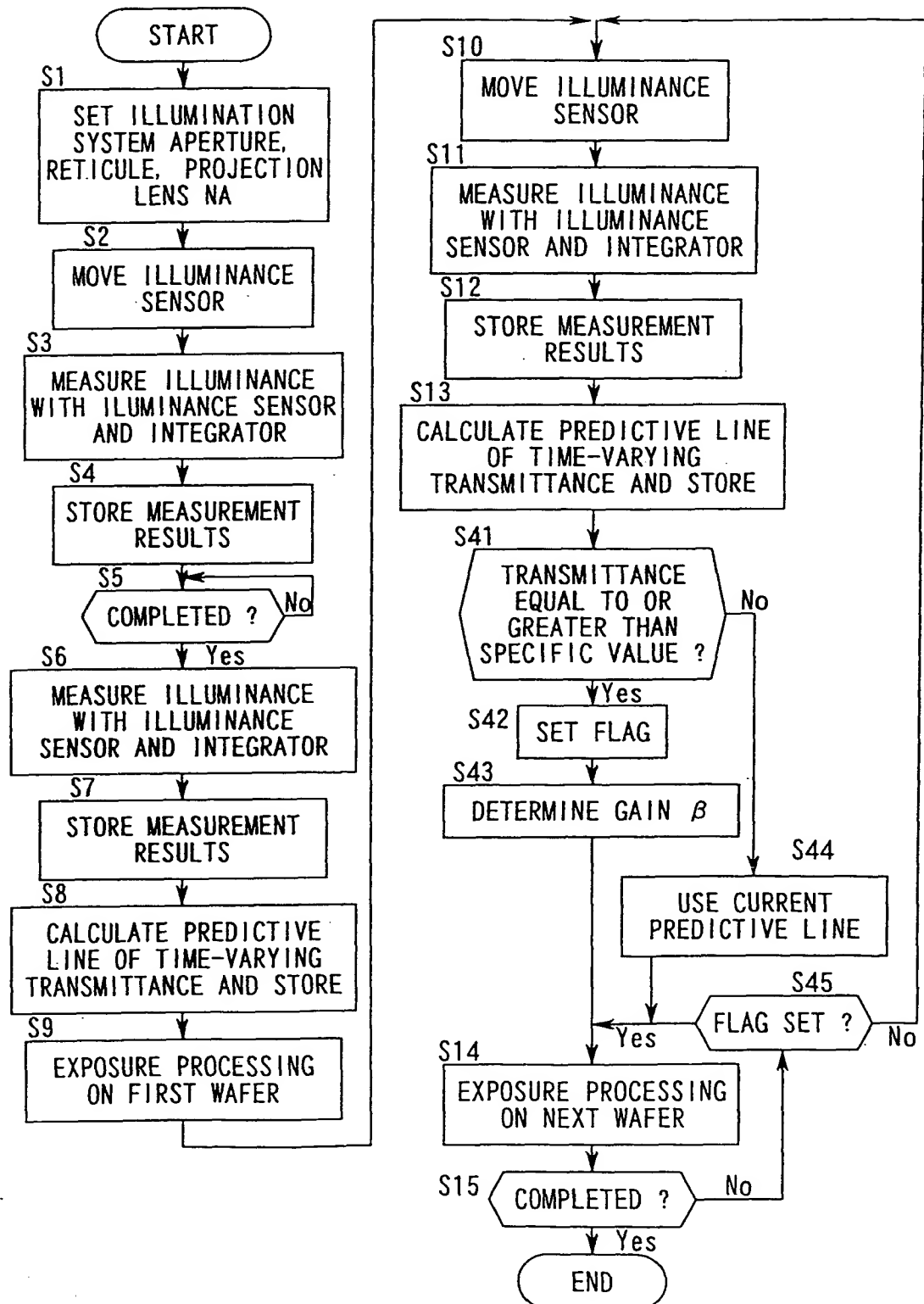


FIG. 11

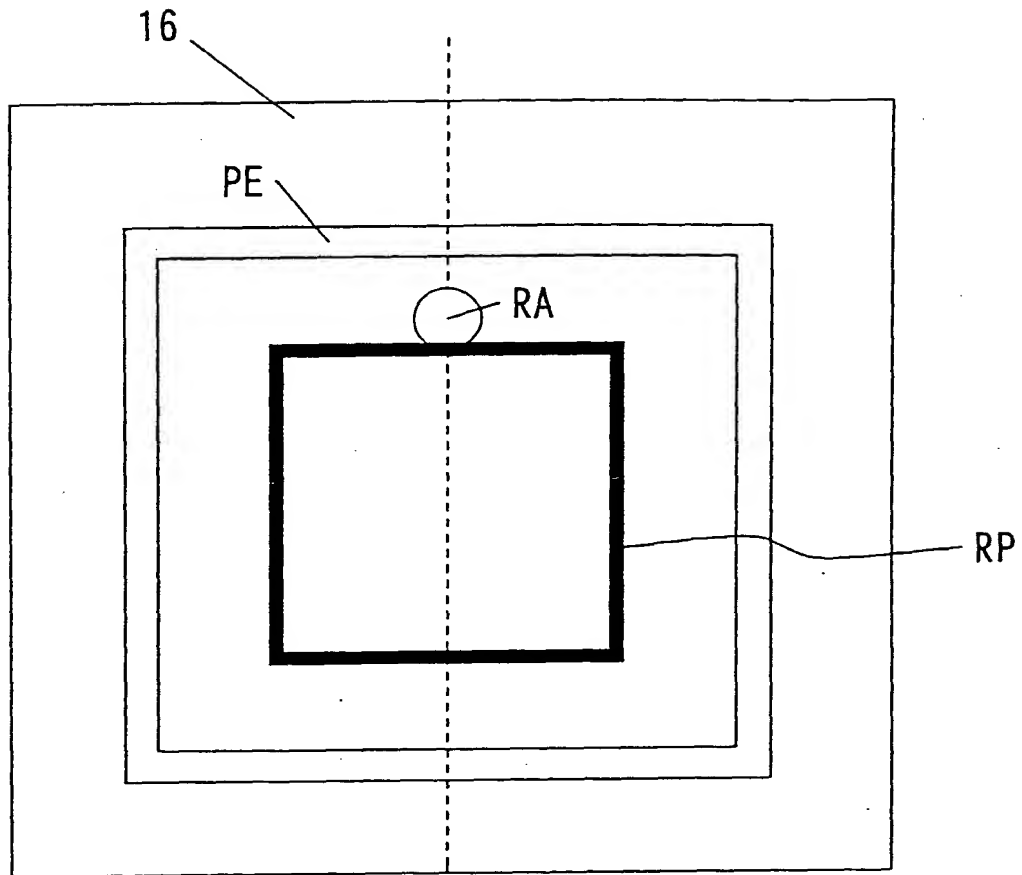


FIG. 12

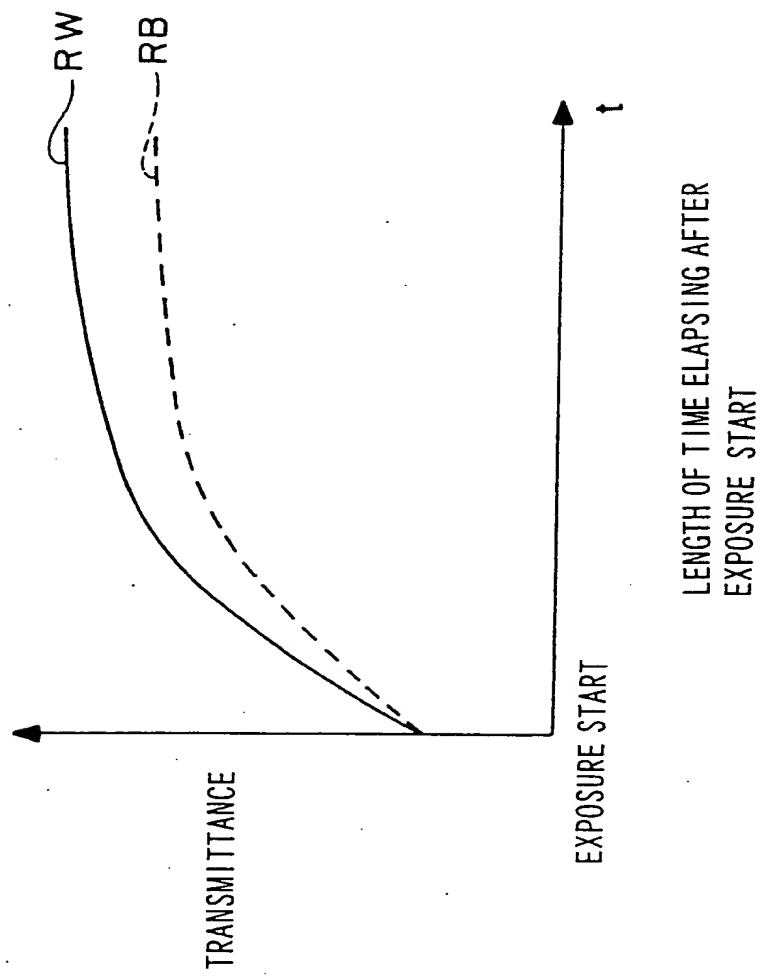


FIG. 13

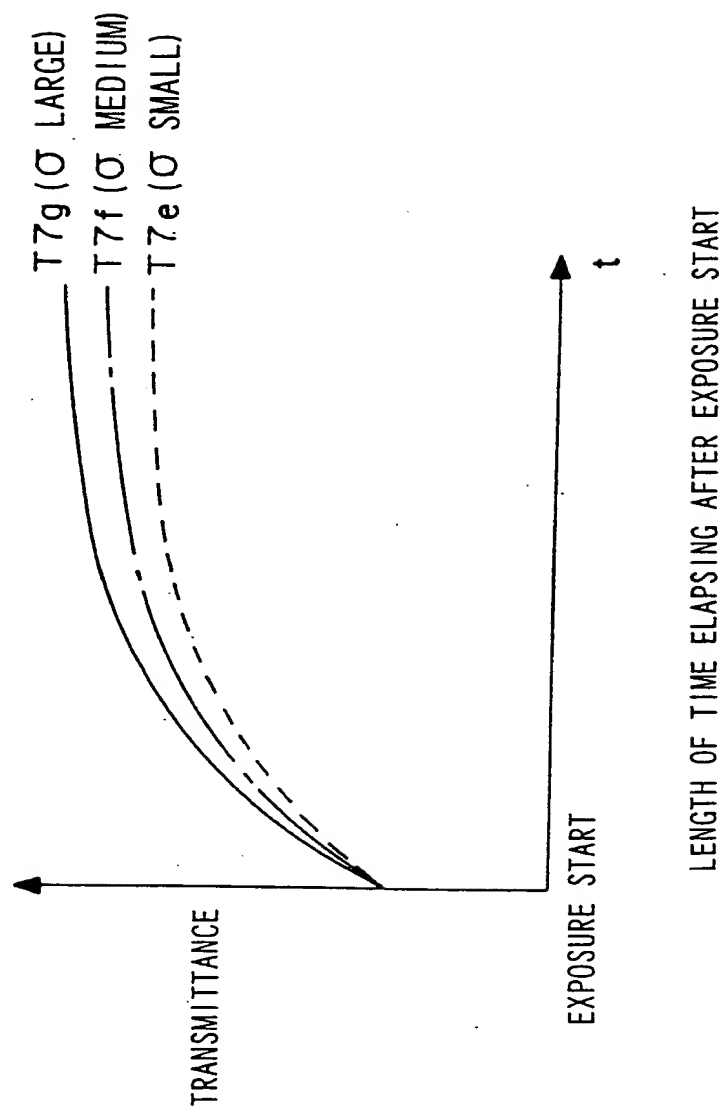


FIG. 14

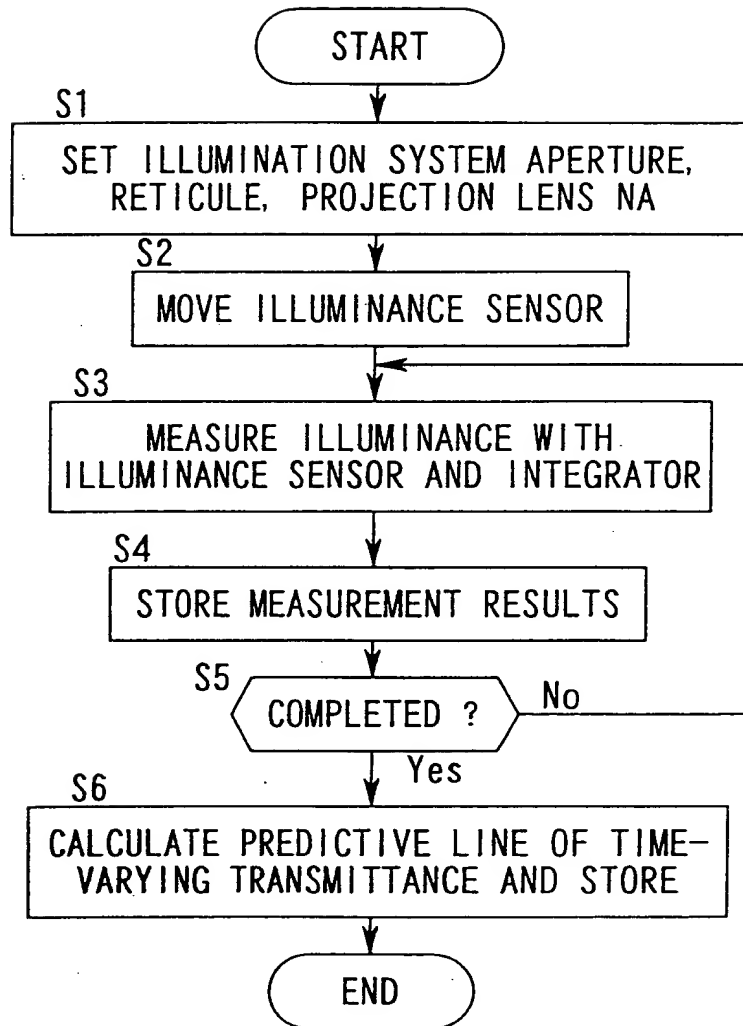
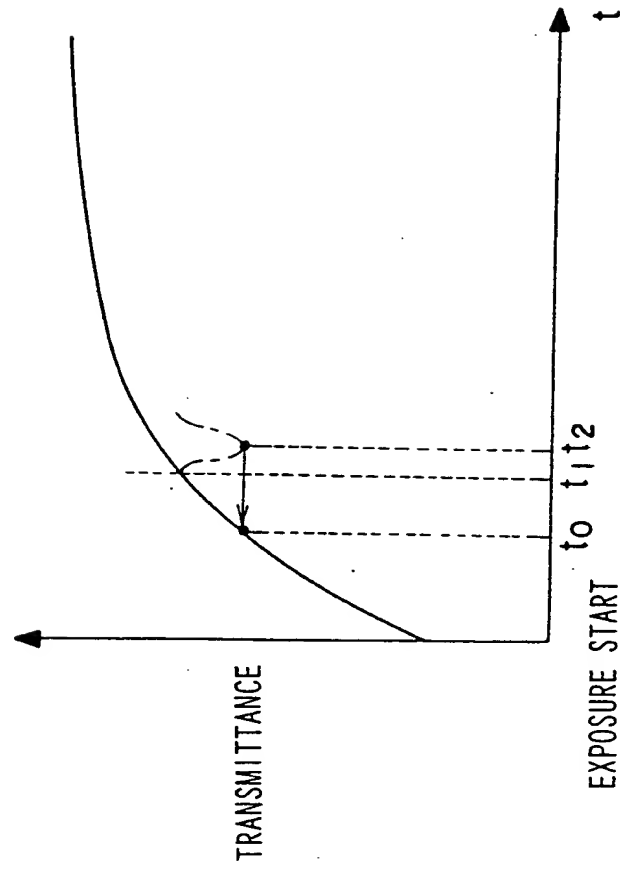
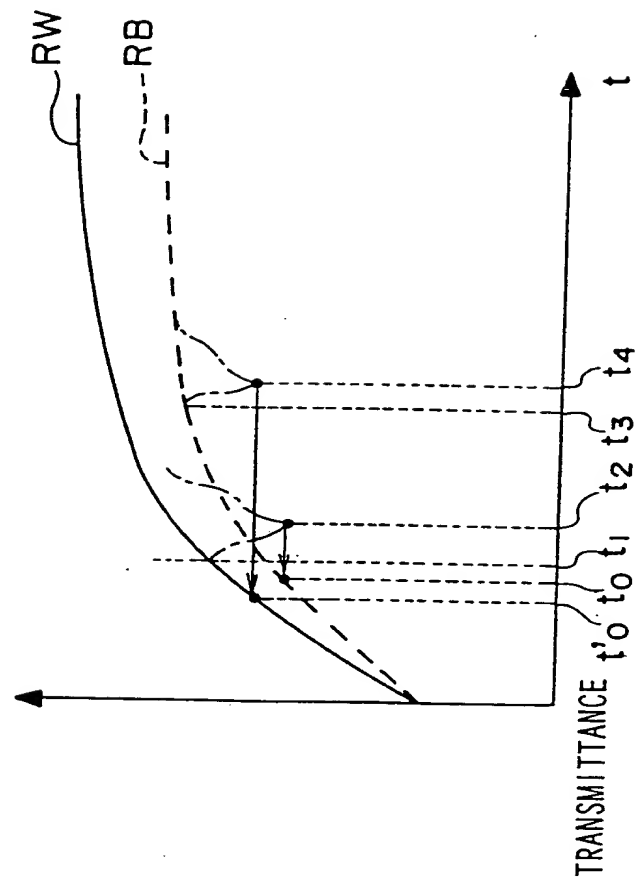


FIG. 15



LENGTH OF TIME ELAPSING AFTER EXPOSURE START

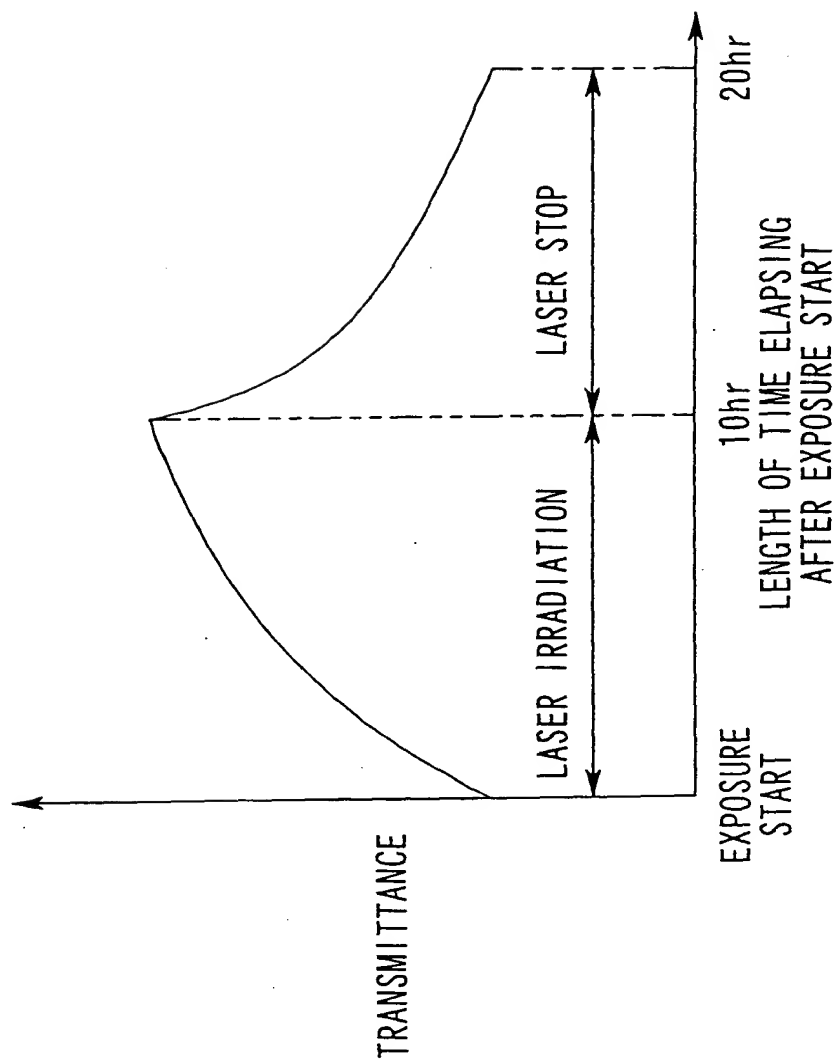
FIG. 16



LENGTH OF TIME ELAPSING AFTER EXPOSURE START



FIG. 17



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